

HAZARDOUS HIGHWALLS – GROUND CONTROL FOR SURFACE MINES

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Fatalities #5 & #6 - April 17, 2007
Fall of Highwall - Surface - Maryland
Tri-Star Mining Inc - Job #3

COAL MINE FATALITY - On Tuesday, April 17, 2007, a 51-year old excavator operator and a 38-year old bulldozer operator, with 15 years and 2 years of mining experience respectively, were fatally injured when a highwall failed. Both miners were operating equipment beneath the highwall measuring approximately 275 feet high, 240 feet wide, and 90 feet deep. The work was being performed near old underground mine works.



Best Practices

GENERAL INFORMATION

Coal Mine Fatal Accident 2007-05 & 06



Operator: Tri-Star Mining, Inc.
Mine: Job #3
Accident Date: April 17, 2007
Classification: Fall of Highwall
Location: Dist. 3, Allegany
County, Maryland
Mine Type: Surface Coal Mine
Employment: 71
Production: 2,100 Tons/Day

MINING SAFETY IS NOT JUST FOR UNDERGROUND MINES!!

- GROUND CONTROL IS VERY IMPORTANT TO SURFACE MINES
- HIGHWALL FAILURES CAN BE DEADLY
- UNDERSTANDING THE ROCK MECHANIC PROPERTIES IS CRUCIAL

How are highwall hazards created?

- ▣ Highwall hazards are created when workers are exposed to highwalls with the potential for failure.
- ▣ It is critical that all impacts to a given highwall are identified, analyzed, and provisions incorporated into the highwall design to account for all potential hazards.

MINIMUM ROCK MECHANIC AND PHYSICAL
FEATURES THAT MUST BE CONSIDERED FOR
HIGHWALL SAFETY:

HIGHWALL DESIGN GEOMETRY

GEOLOGIC STRUCTURE

ROCK FRACTURING PATTERNS

HYDROGEOLOGIC CONDITIONS

HIGHWALL DESIGN GEOMETRY

Typical Highwall



GEOLOGIC STRUCTURE



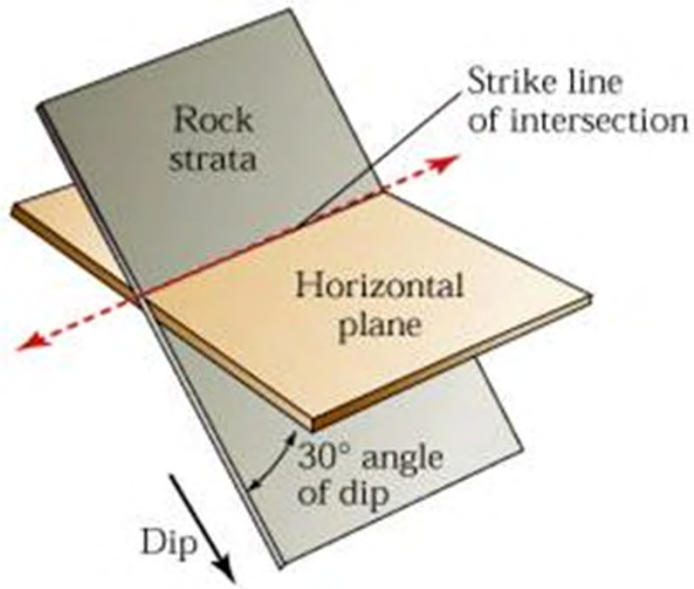
A little geometry: A plane can be defined by two lines

For geology, we use either

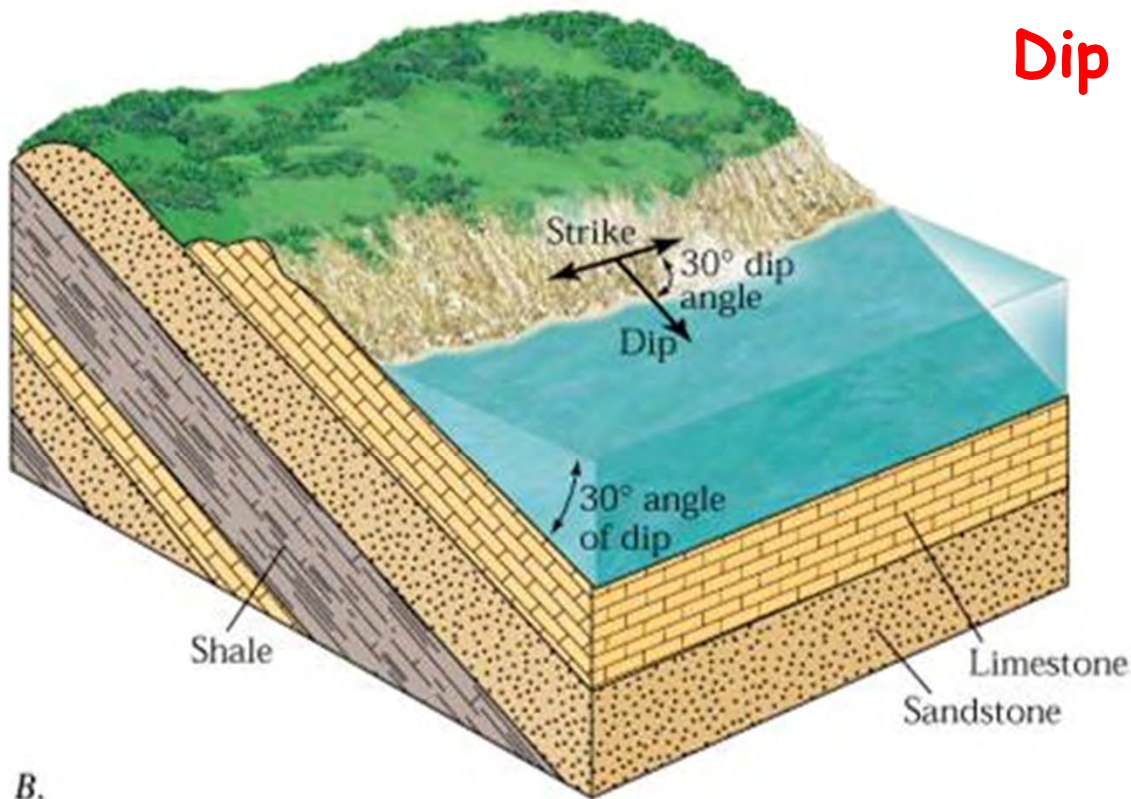
-Strike and Dip

or

-Dip and Dip direction



A.

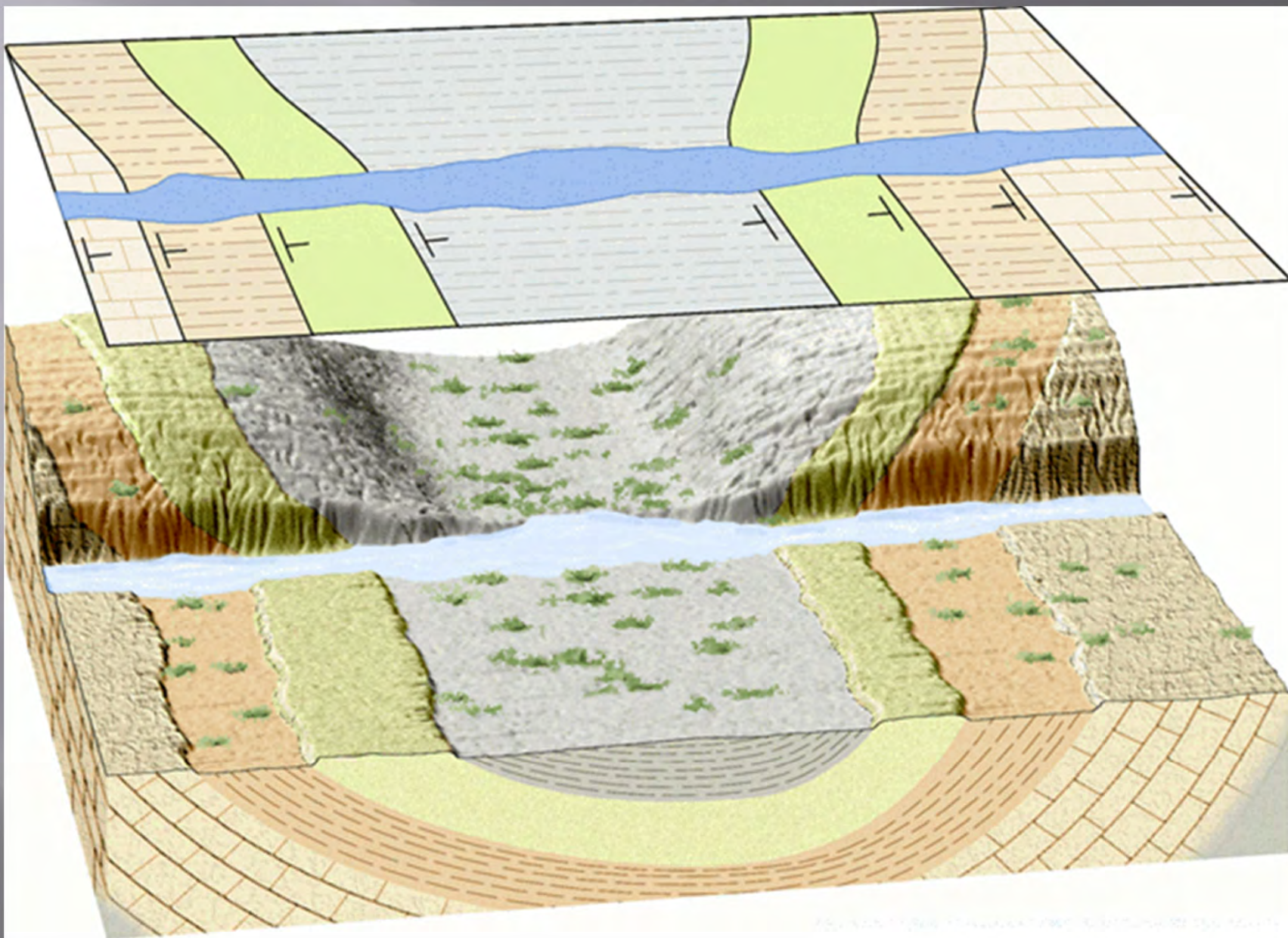


B.

Strike - Direction of horizontal line in a dipping

Dip - The true maximum of a bed measured horizontal

Dip Direction - Direction of the maximum dip; also from strike



ROCK MECHANICS DISCONTINUITIES:

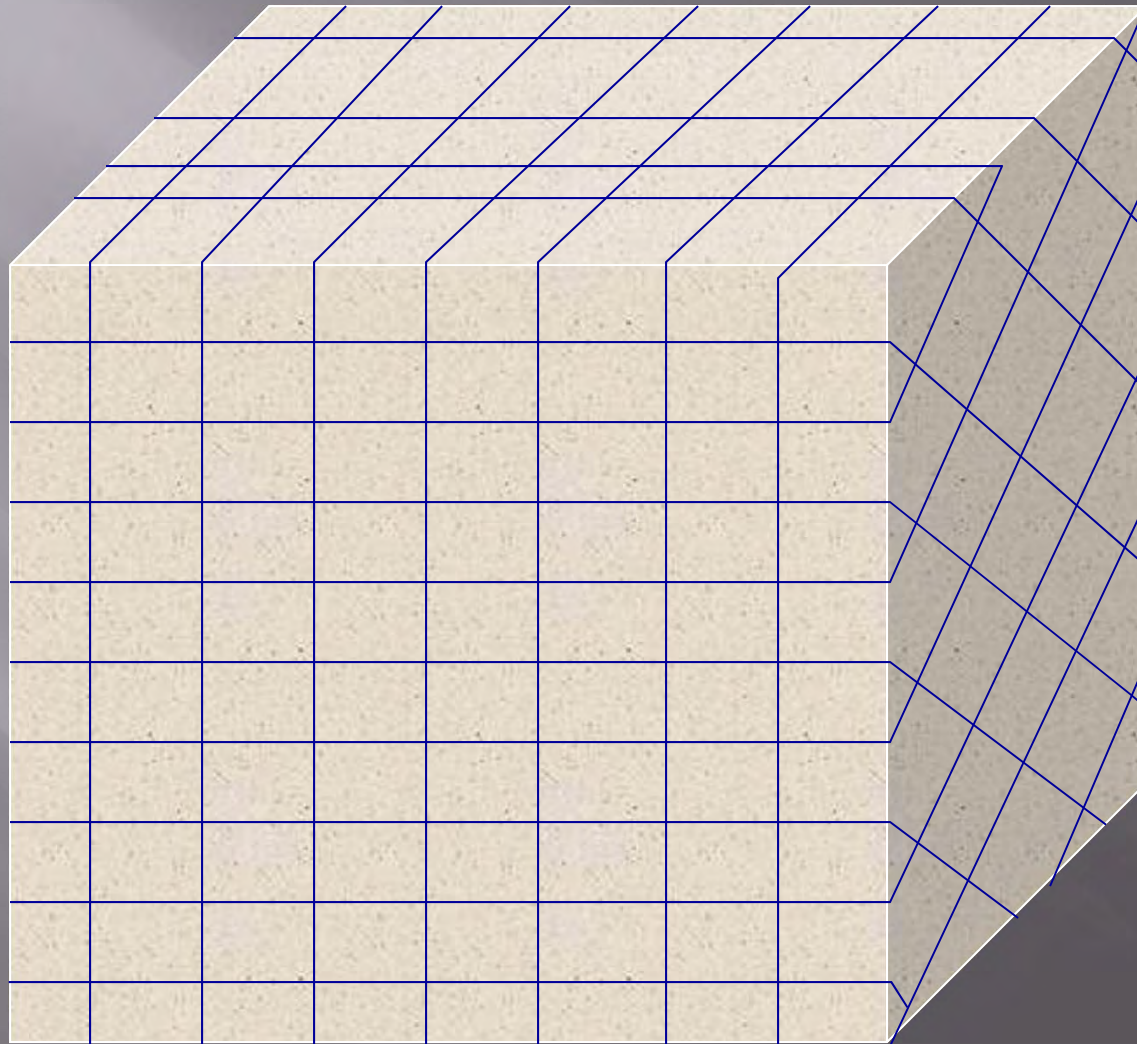
BEDDING
JOINTS
FRACTURES

GENERALLY THE HIGHWALL
ROCK MASS PROPERTIES CAN
DIFFER GREATLY FROM THE
INTACT INDIVIDUAL ROCK
BLOCKS

Discontinuities

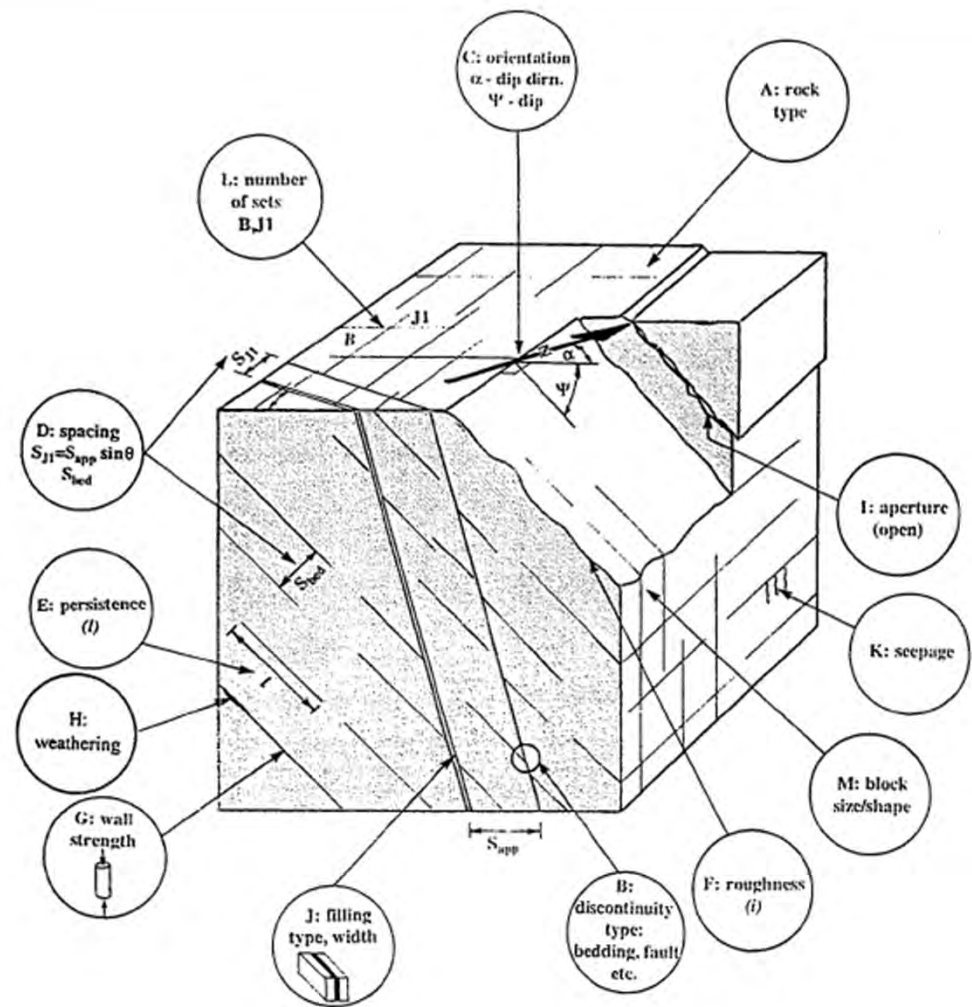
- ▣ A discontinuity is defined as a disconnect in the continuity of rock material.
- ▣ It creates a weak structural plane where movement and failure can occur.

Effect of Discontinuities on Intact Rock



Properties of Discontinuities

- Orientation
- Spacing
- Persistence
- Roughness
- Aperture
- Infilling
- Seepage
- Number of Sets
- Block Size



Obtaining Data on Discontinuities

- ▣ Field mapping
- ▣ Core drilling



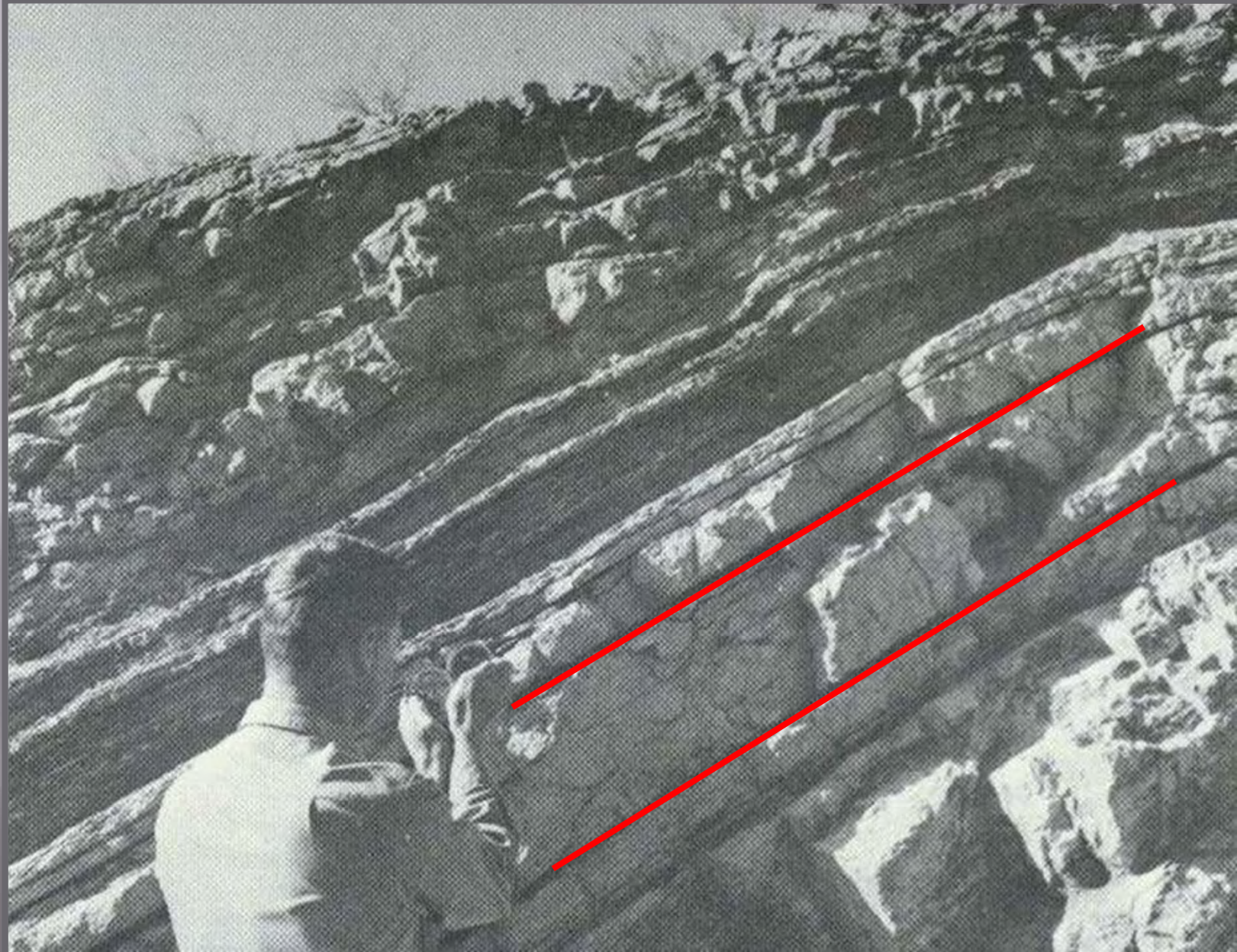


Bedding

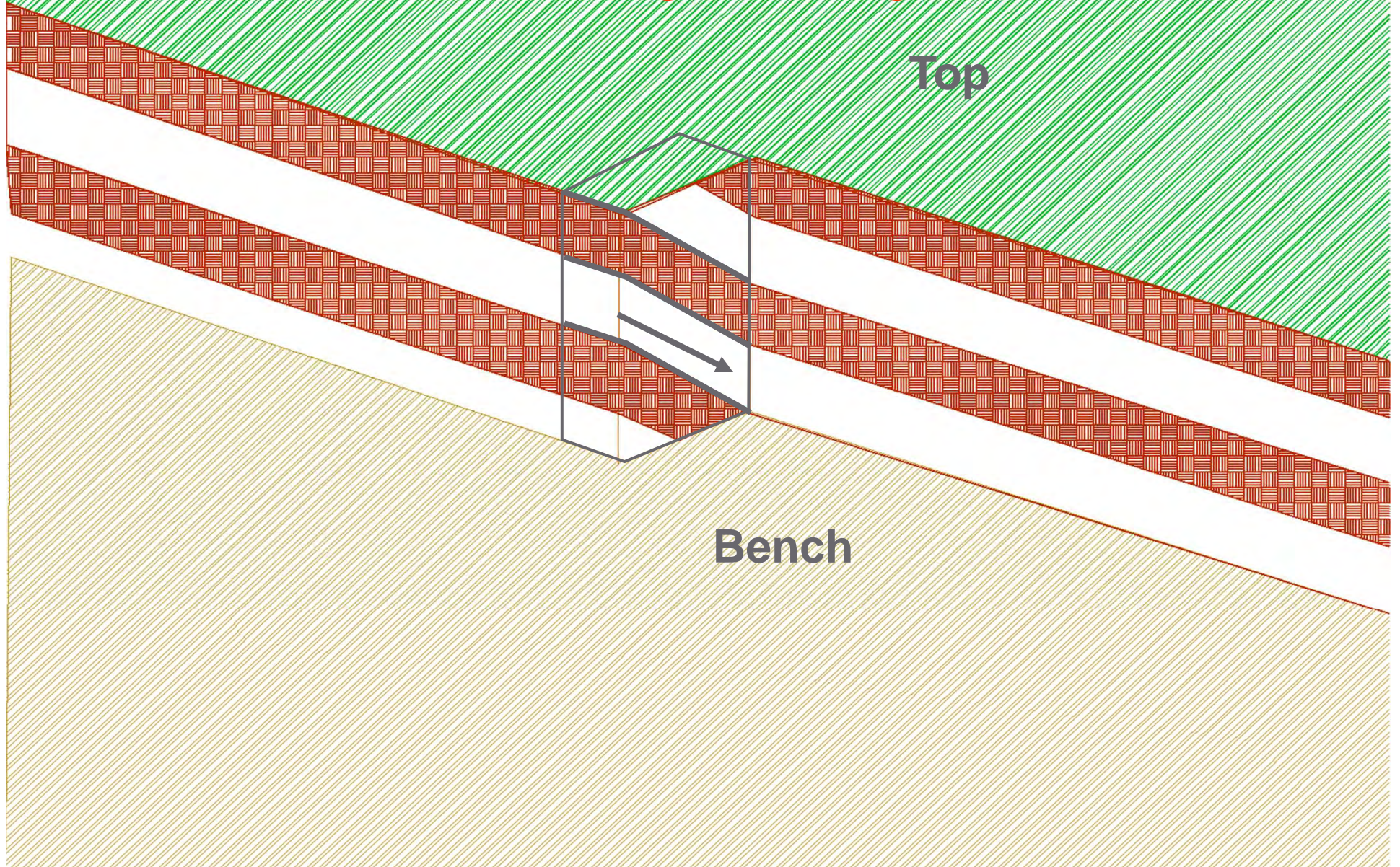
Bedding



Moderately Dipping Bedding



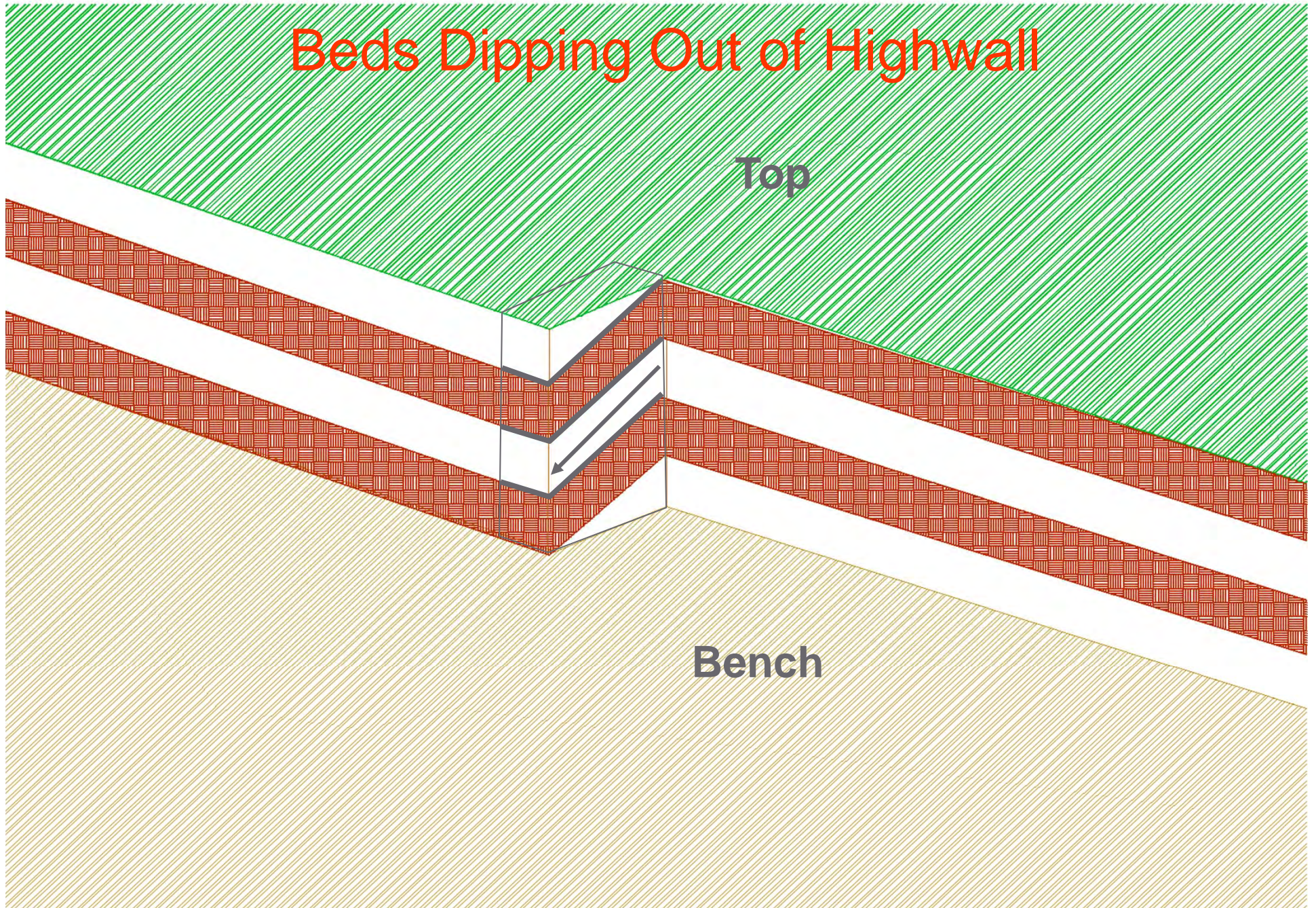
Favorable Orientation Beds Dipping Into Highwall



Top

Bench

Unfavorable Orientation Beds Dipping Out of Highwall



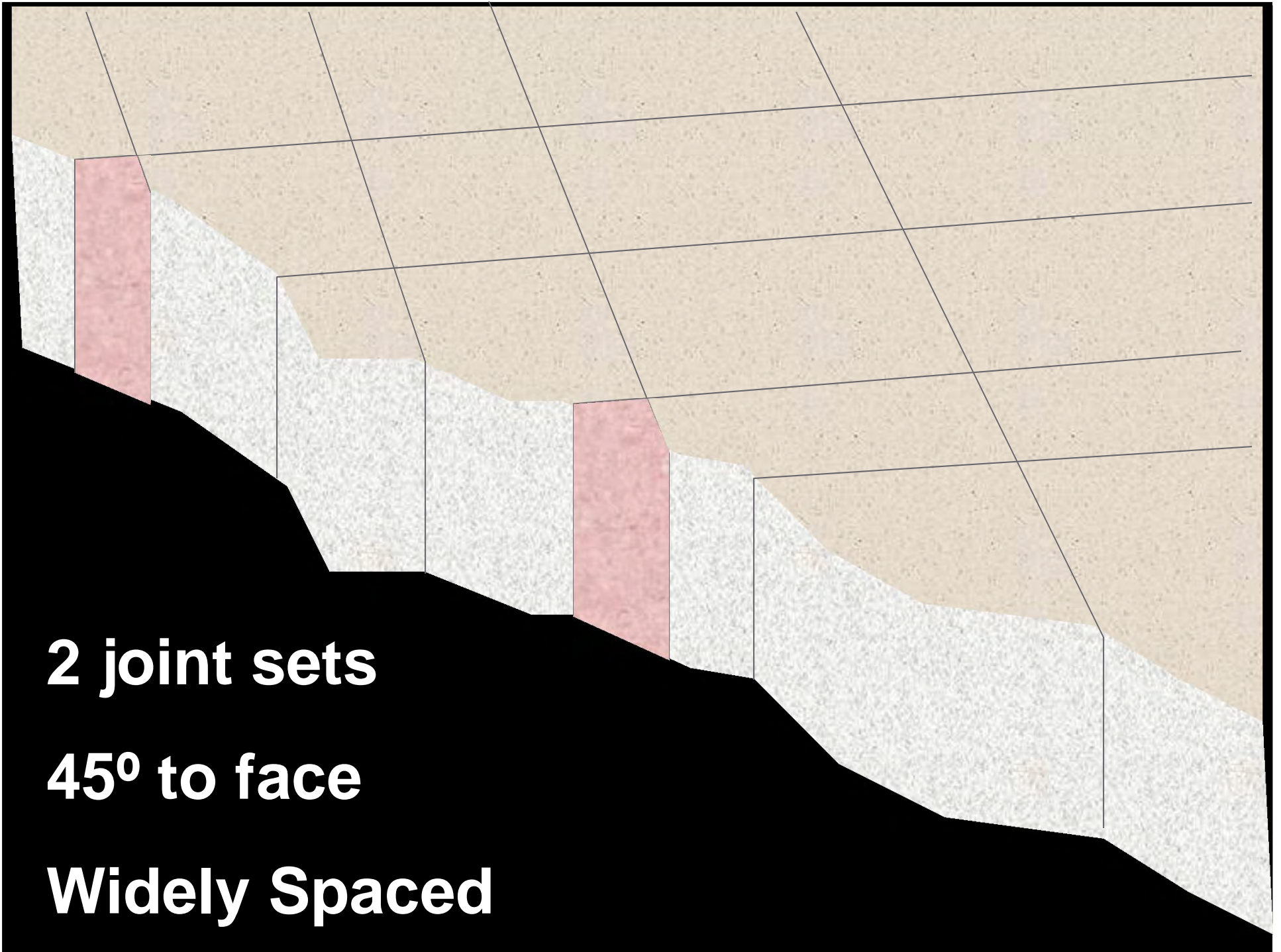
Joints

Joints



Two Sets of Vertical Joints (3-D)

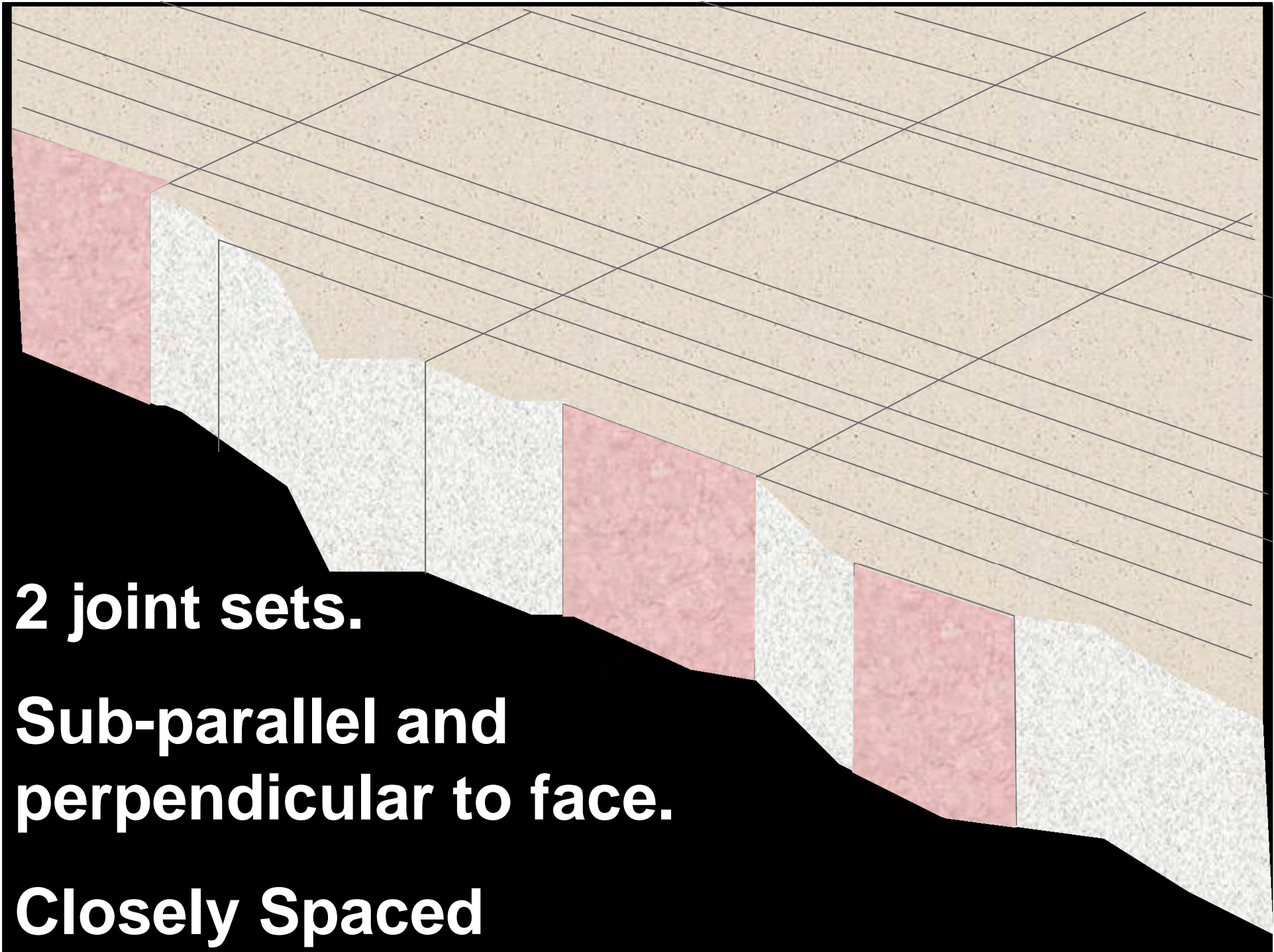




2 joint sets

45° to face

Widely Spaced



2 joint sets.

**Sub-parallel and
perpendicular to face.**

Closely Spaced

Non-Perpendicular Joint Intersection Near Face

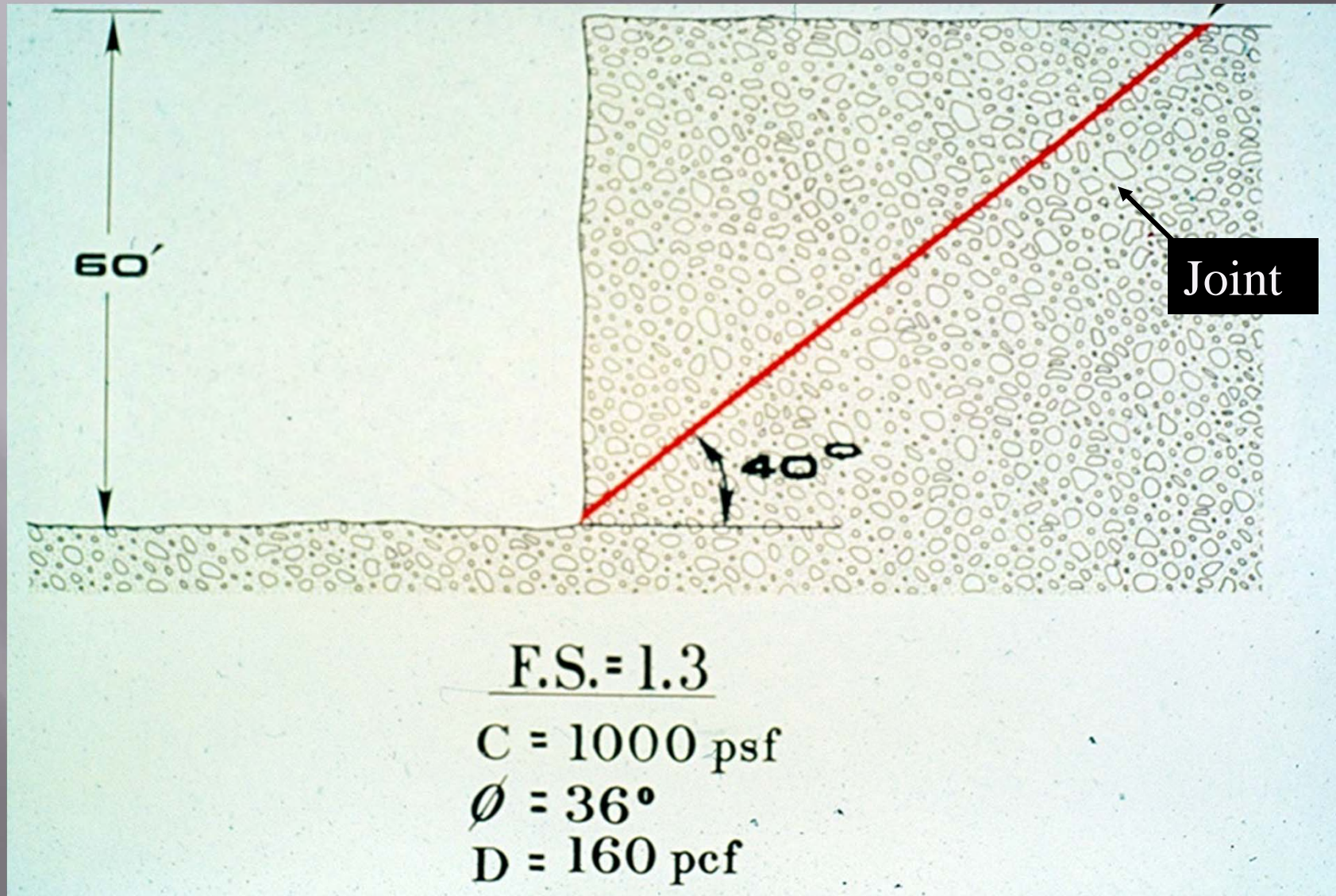


HYDROGEOLOGIC CONDITIONS

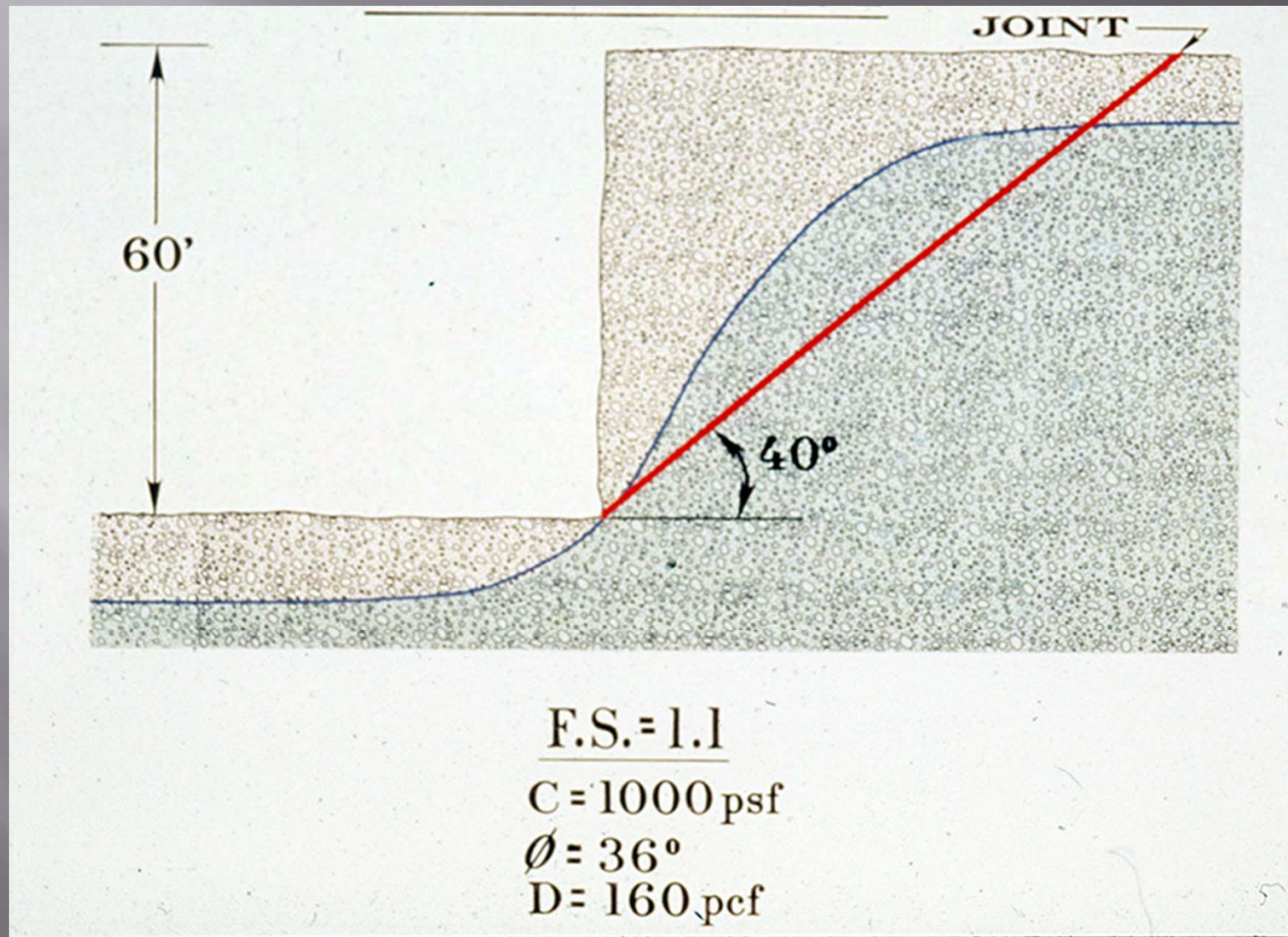
Seepage

- ▣ Water is often a contributing factor to highwall failures.
- ▣ Effects of water:
 - adds weight to the potential sliding mass
 - reduces strength of soil/rock
 - erodes supporting material
 - provides driving force in joints

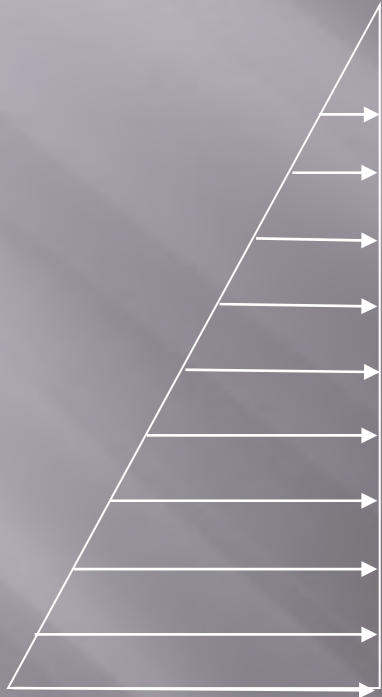
Dry Highwall FS=1.3



Saturated Highwall FS = 1.1

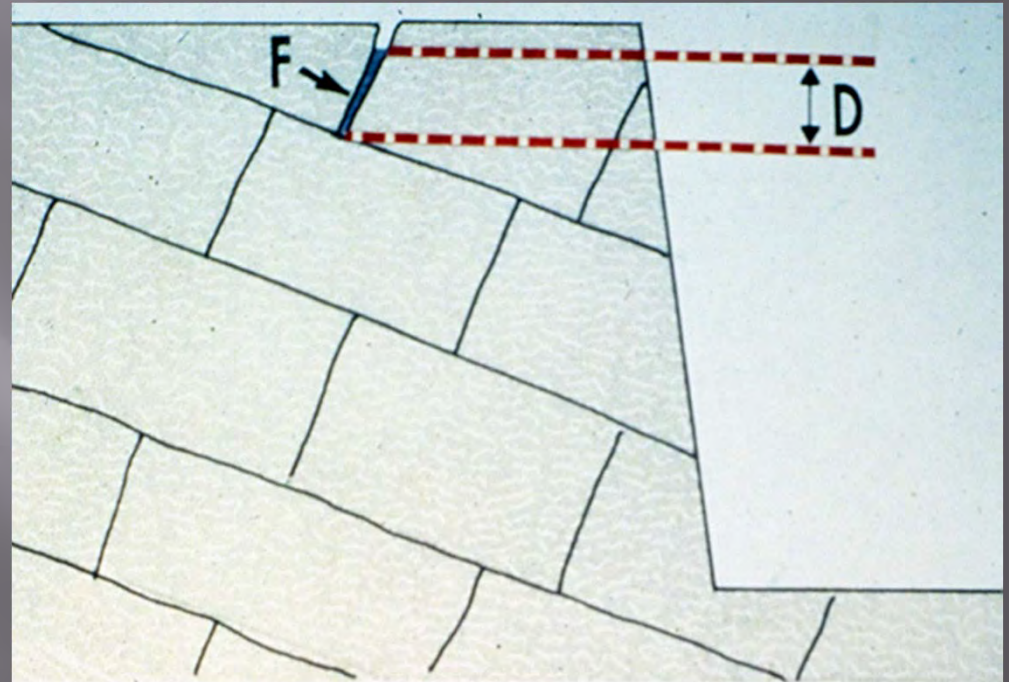


Water Pressure in Joints



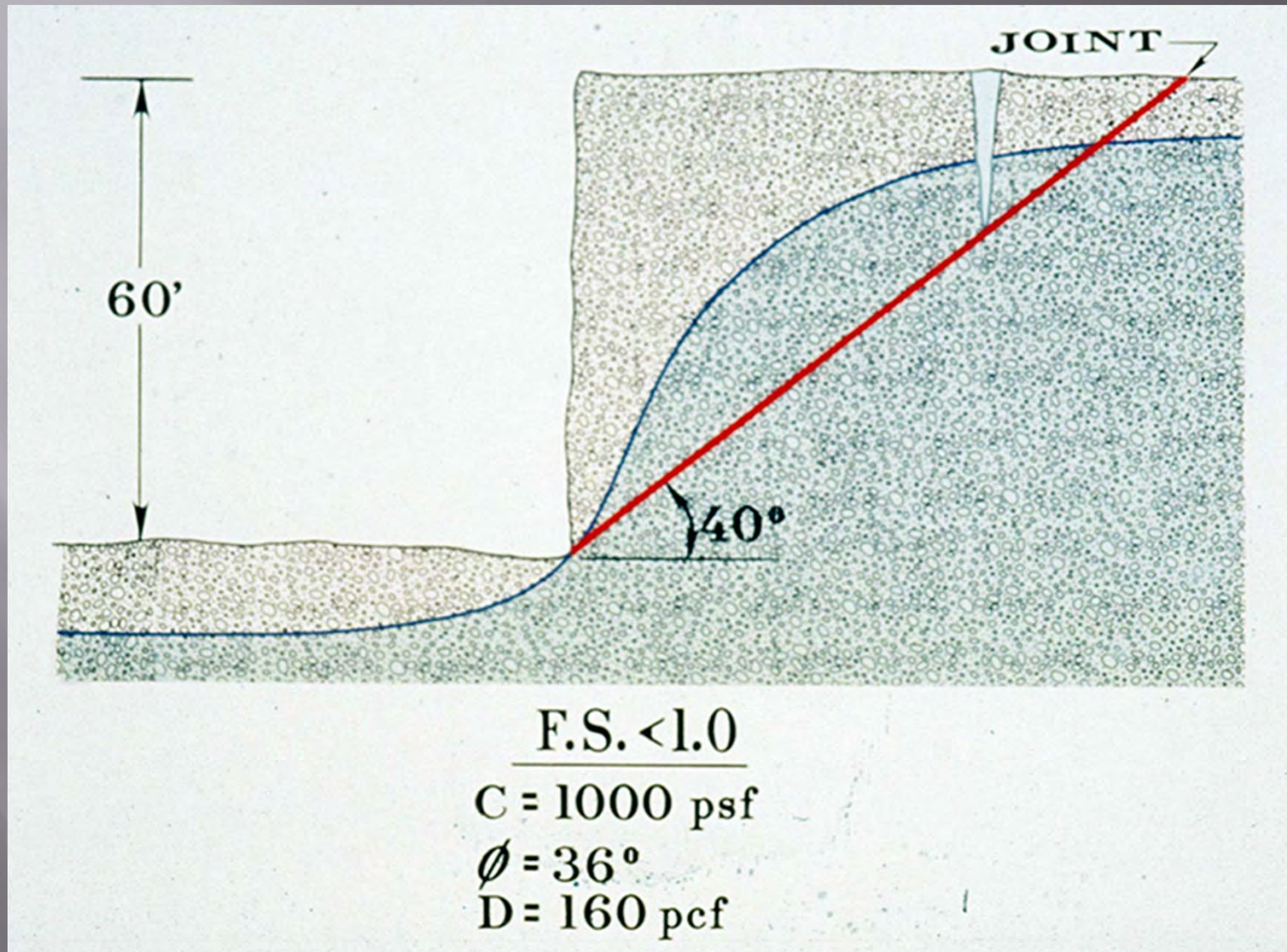
$$P_{\max} = 62.4 \times \text{depth}$$

$$F = 0.5(P_{\max} \times \text{depth}) / 2000$$



| | | |
|--------------------|-----|------|
| DEPTH, D, FEET | 10 | 20 |
| MAX. PRESSURE, PSF | 624 | 1248 |
| FORCE, TONS | 1.5 | 6.2 |

Saturated Highwall with Water Column FS < 1.0

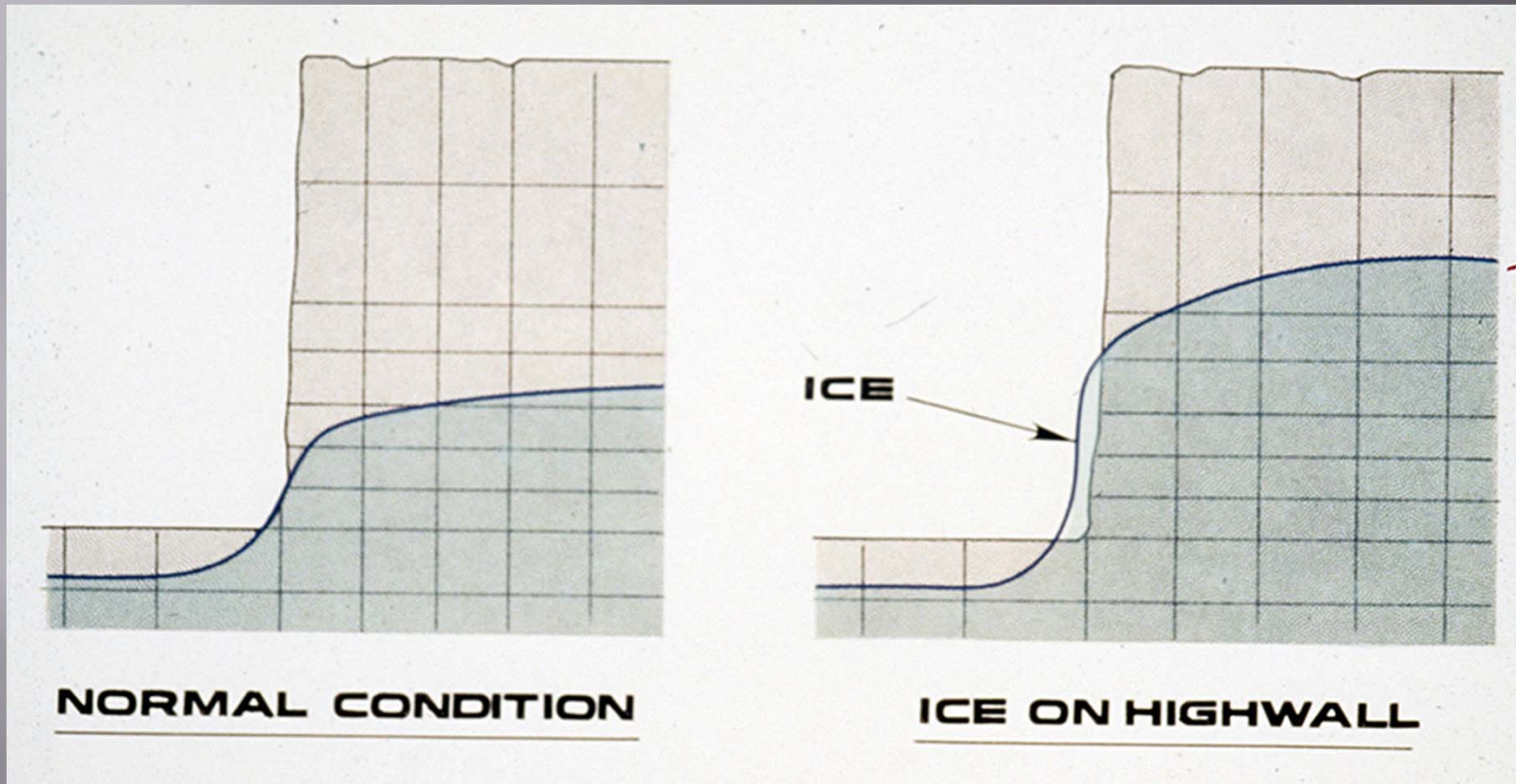


Ice is a Common Sight on Highwalls

- It identifies seepage locations.



Effects of Ice



- The ice acts as a dam on the face of the highwall which raises the internal water elevation.
- The ice also adds weight to the wall.

HIGHWALL FAILURE MODES

Rock Mass Failure Modes

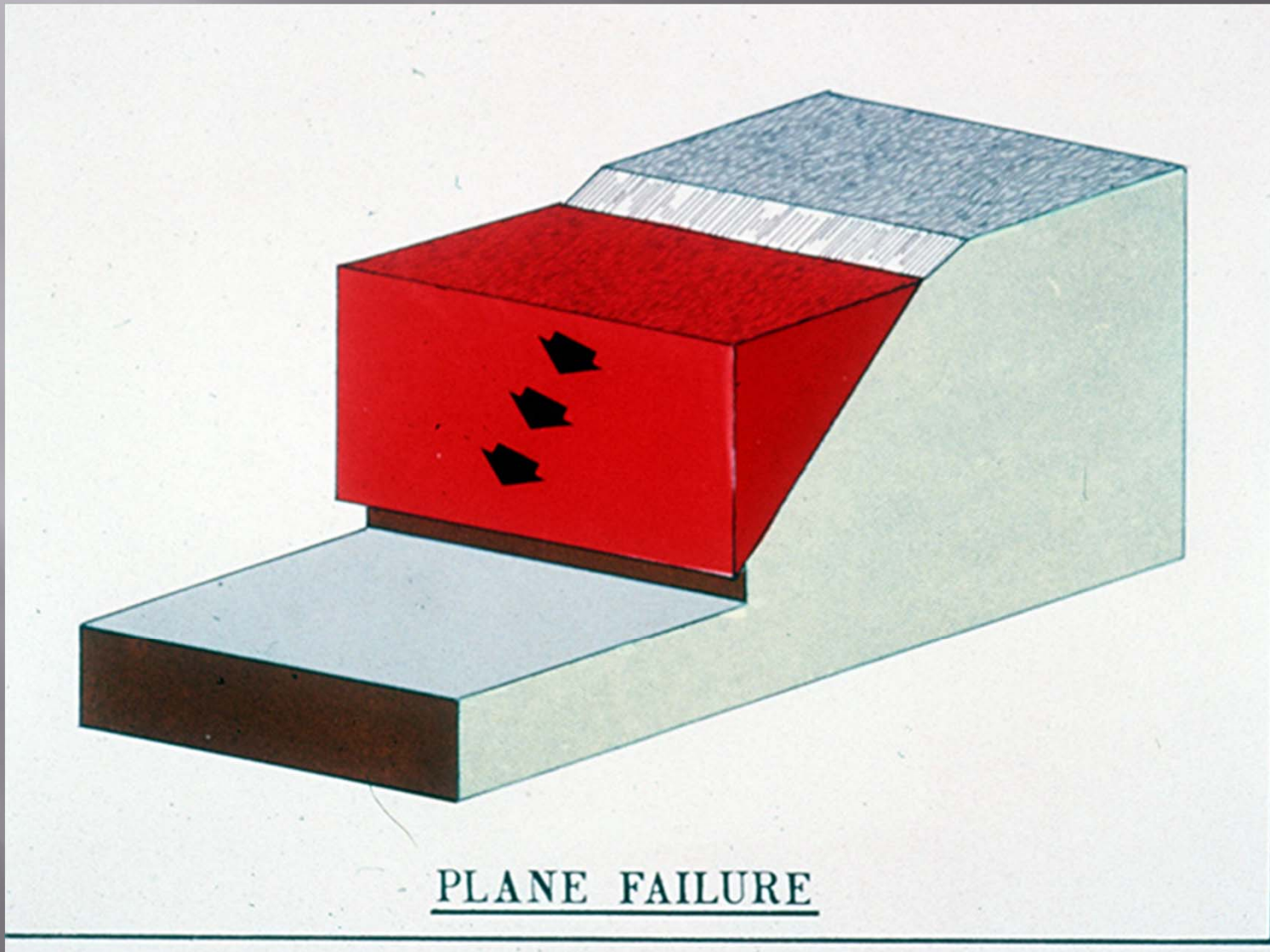
- ▣ Planar
- ▣ Wedge
- ▣ Toppling
- ▣ Circular



Rock Mass Failure



Planar Failure



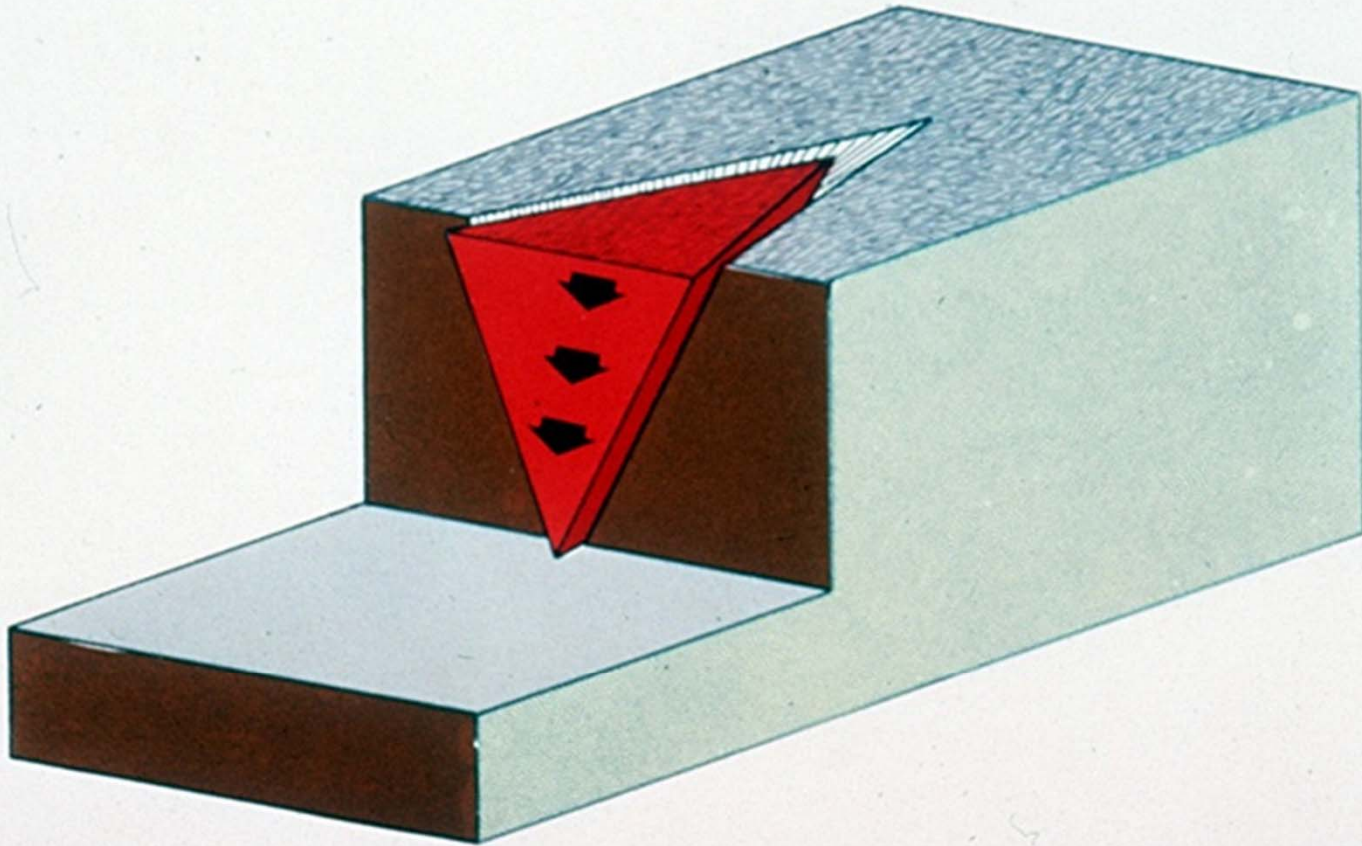
Planar Failure

- ▣ Planar failures involve sliding movement along a single discontinuity surface; however, additional discontinuities typically define the lateral extent of the failures.

Planar Failure

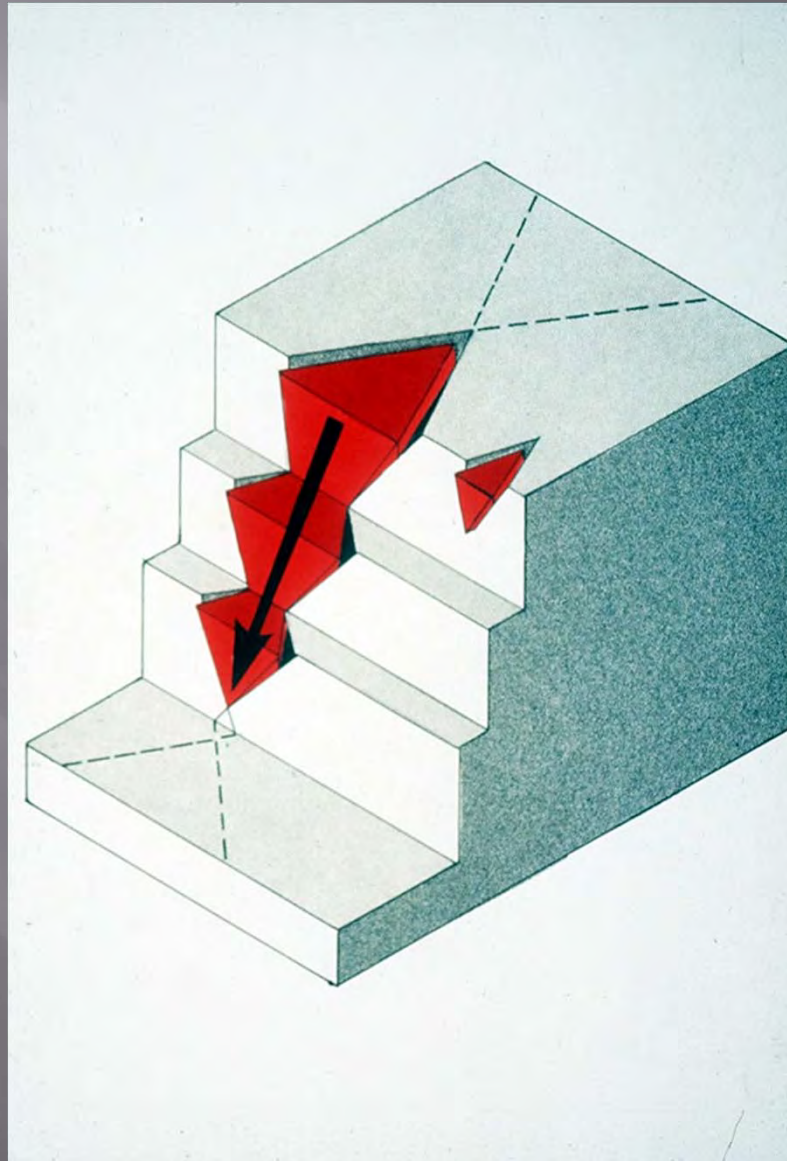


Wedge Failure



WEDGE FAILURE

Wedge Failure



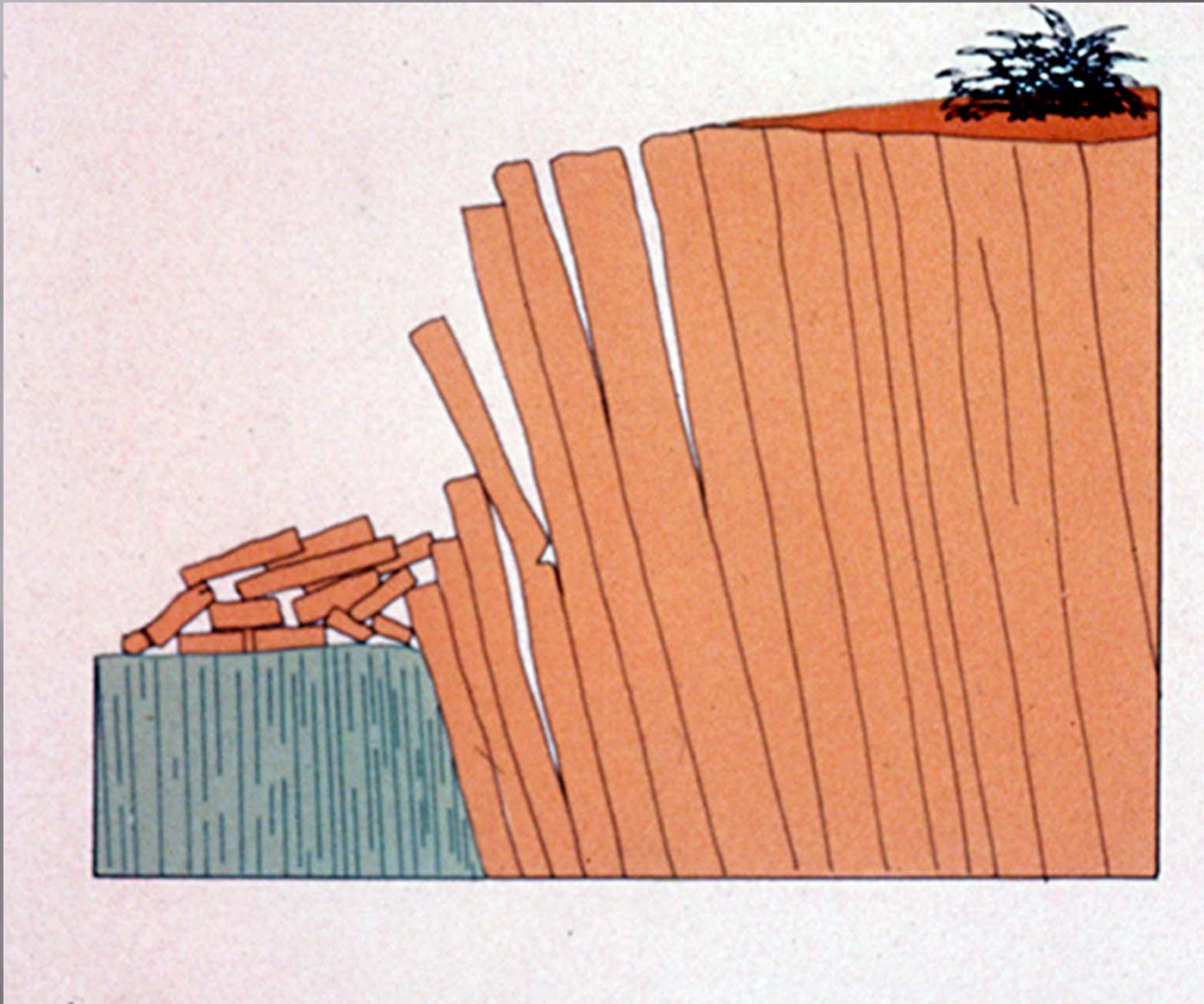
Wedge Failure

- ▣ Wedge failures involve sliding movement along two discontinuity surfaces that intersect at an angle forming a wedge shaped block in the highwall face.

Wedge Failure



Toppling Failure



Toppling Failure

- ▣ Toppling failures involve rotational movement around the base of a slab or column formed by steeply dipping discontinuities oriented parallel or sub-parallel to the highwall face.

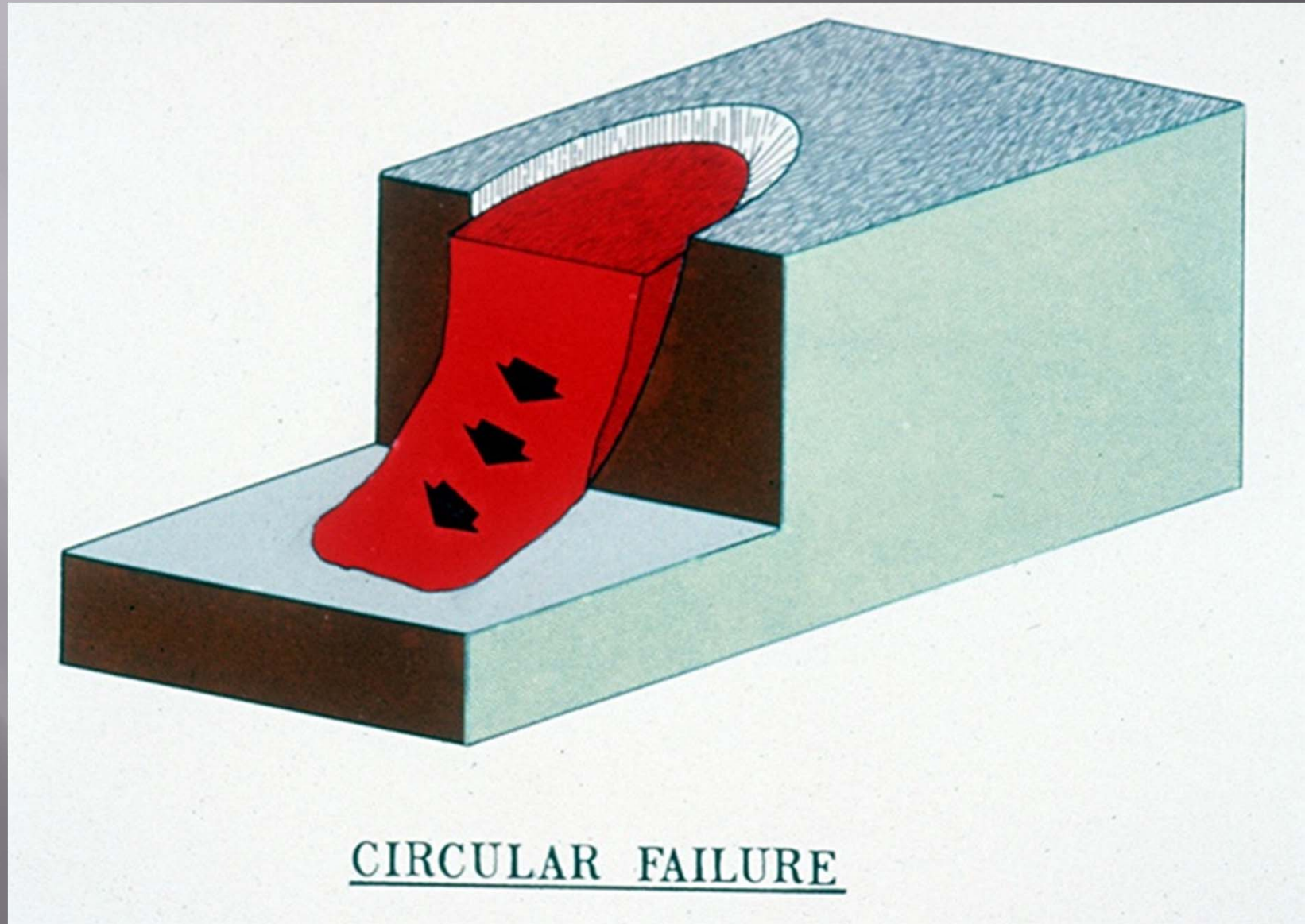
Non-Fatal Toppling Failure Accident



Non-Fatal Toppling Failure Accident



Circular Failure



Circular Failure

- ▣ Circular failures involve rotational and sliding movement along a failure surface. Circular failures are not common in small highwall situations $< 100'$. However, circular failures can and have occurred when highwalls are oriented near or parallel to fractures.

Circular Failure – Before



Circular Failure - After



Rock Falls



GENERAL
INFORMATION

Coal Mine Fatal Accident 2006-35



| | |
|-----------------|------------------------------------|
| Operator: | Hendrickson Equipment, Inc. |
| Mine: | Smith Branch No. 1 |
| Accident Date: | July 18, 2006 |
| Classification: | Fall of Highwall |
| Location: | Dist. 6, Knott County, Kentucky |
| Mine Type: | Surface Coal Mine |
| Employment: | 7 |
| Production: | 150 Tons/Day |

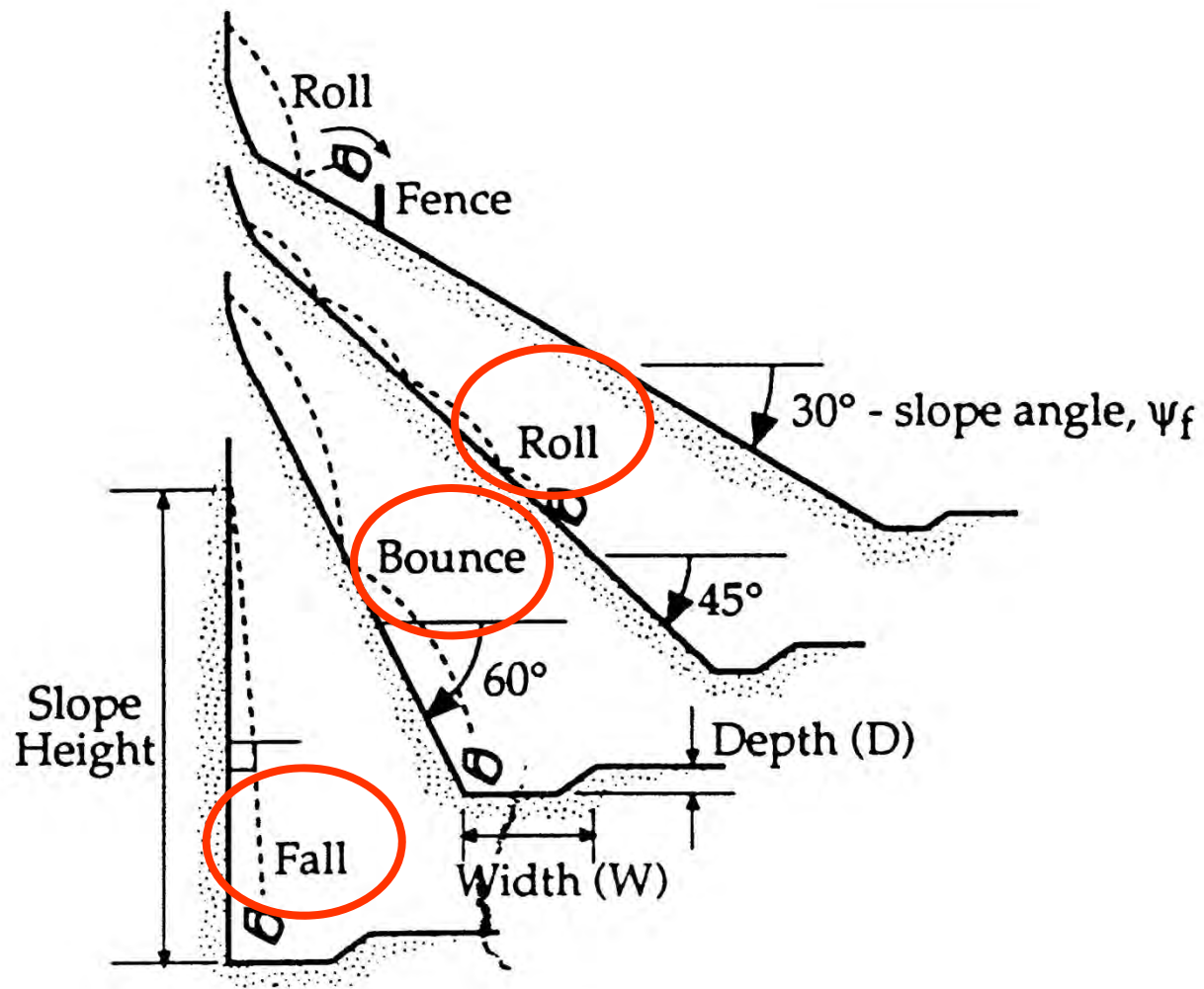


Rock Fall Energy

| Height of Fall (feet) | Approx. Weight (lbs) | Equivalent Cube Size (inches) | Max. Speed (mph) | Kinetic Energy (ft-lbs) | Approx. Force of Impact ^[1] (lbs) |
|-----------------------|----------------------|-------------------------------|------------------|-------------------------|--|
| 50 | 2.5 | 3 | 39 | 125 | 500 |
| 100 | 2.5 | 3 | 55 | 250 | 1,000 |
| 125 | 2.5 | 3 | 61 | 313 | 1,250 |
| 160 | 2.5 | 3 | 69 | 400 | 1,600 |
| 50 | 20 | 6 | 39 | 1000 | 4,000 |
| 100 | 20 | 6 | 55 | 2000 | 8,000 |
| 125 | 20 | 6 | 61 | 2500 | 10,000 |
| 160 | 20 | 6 | 69 | 3200 | 12,800 |

[1] Assuming that the ground surface is soft enough that the rock penetrates the ground surface 3-inches upon impact. A smaller penetration results in a larger force of impact.

Effects of Highwall Geometry on Rock Fall



(Ritchie 1963)

Highwall Geometry

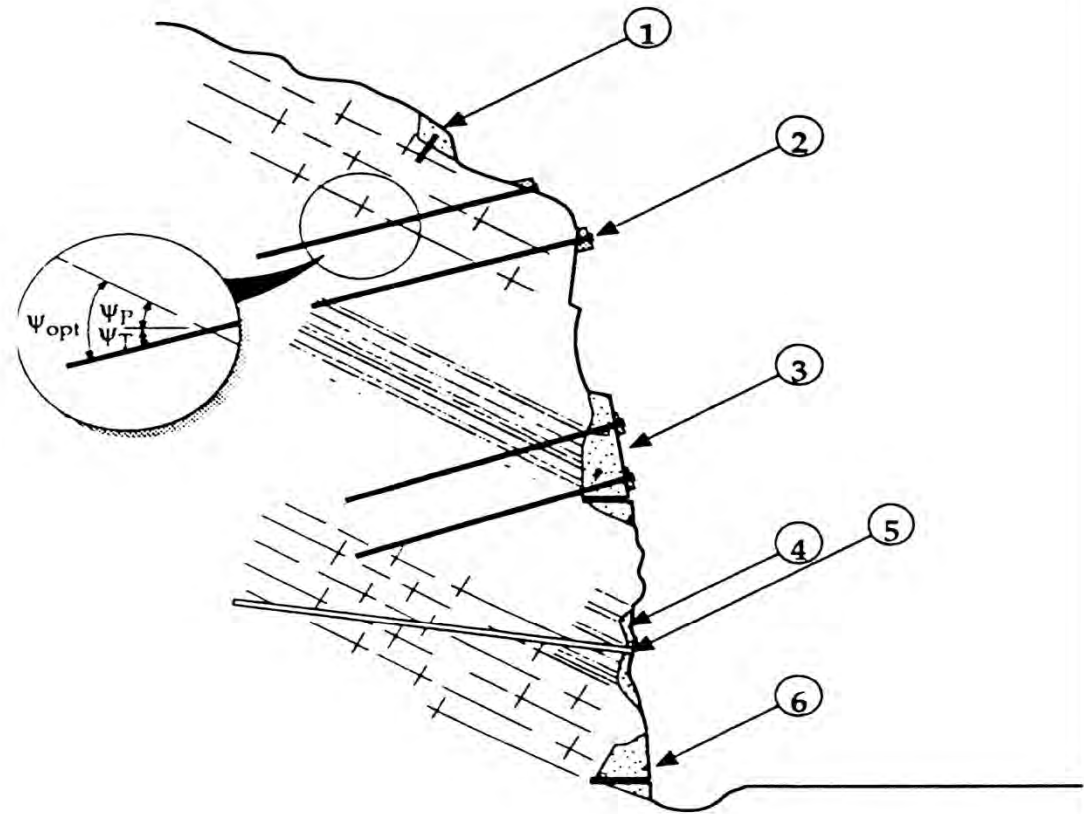


Launch Feature



REMEDIATING THE HAZARD

Rock reinforcement methods for highwall stabilization.



- ① Reinforced concrete dowel to prevent loosening of slab at crest
- ② Tensioned rock anchors to secure sliding failure along crest
- ③ Tieback wall to prevent sliding failure on fault zone
- ④ Shotcrete to prevent raveling of zone of fractured rock
- ⑤ Drain hole to reduce water pressure within slope
- ⑥ Concrete buttress to support rock above cavity

(TRB 1996)

Rock Anchors



Shotcrete Face



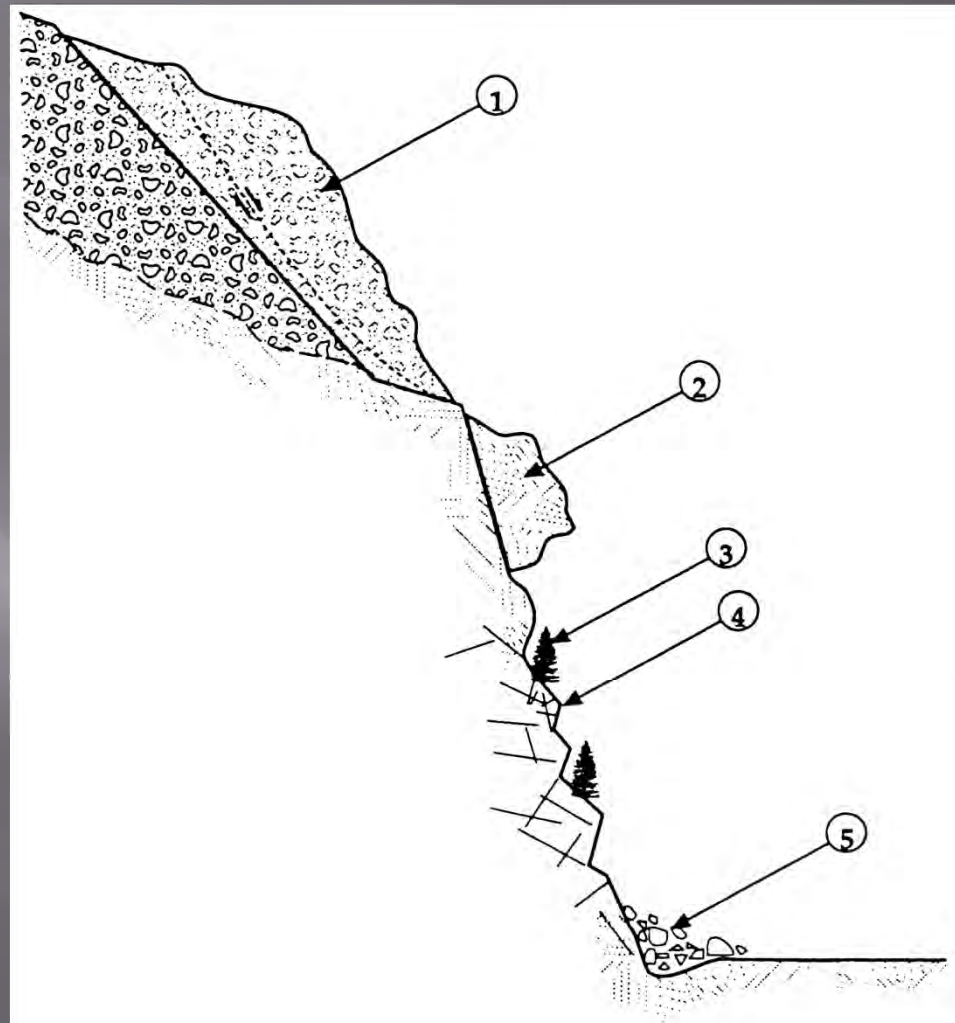
Drainage

- ▣ If a water problem is expected, defensive measures can be taken:
 - Grouting to prevent infiltration,
 - Diversion ditches above the highwall to prevent surface runoff,
 - Vertical wells behind the highwall crest, and
 - Horizontal drains in the highwall face.

Rock Removal

- ▣ The goal of rock removal is to remove potentially loose rock from the face of the highwall.
- ▣ Rock removal is preferred over rock reinforcement when a stable face can be achieved.
- ▣ Pre-splitting during blasting helps reduce broken rock in highwall face.

Rock removal methods for highwall stabilization.



- ① Resloping of unstable weathered material in upper part of slope
- ② Removal of rock overhang by trim blasting
- ③ Removal of trees with roots growing in cracks
- ④ Hand scaling of loose blocks in shattered rock
- ⑤ Clean ditch

(TRB 1996)

Scalers Supported by Ropes



Pre-Splitting Highwall



Mechanical Scaling

- ▣ Mechanical scaling is generally considered to be scaling by heavy equipment.
- ▣ It is not very selective and will generally only remove excessively loose material.
- ▣ It may also cause damage to the highwall, creating more loose material in the process.
- ▣ Dragging the face of the highwall with a chain or similar object is marginally effective at best.

Scaling Chain



Dragging the Face



Scaling with Crane



Scaling with Excavator



Mesh on Highwall



Catch Fence

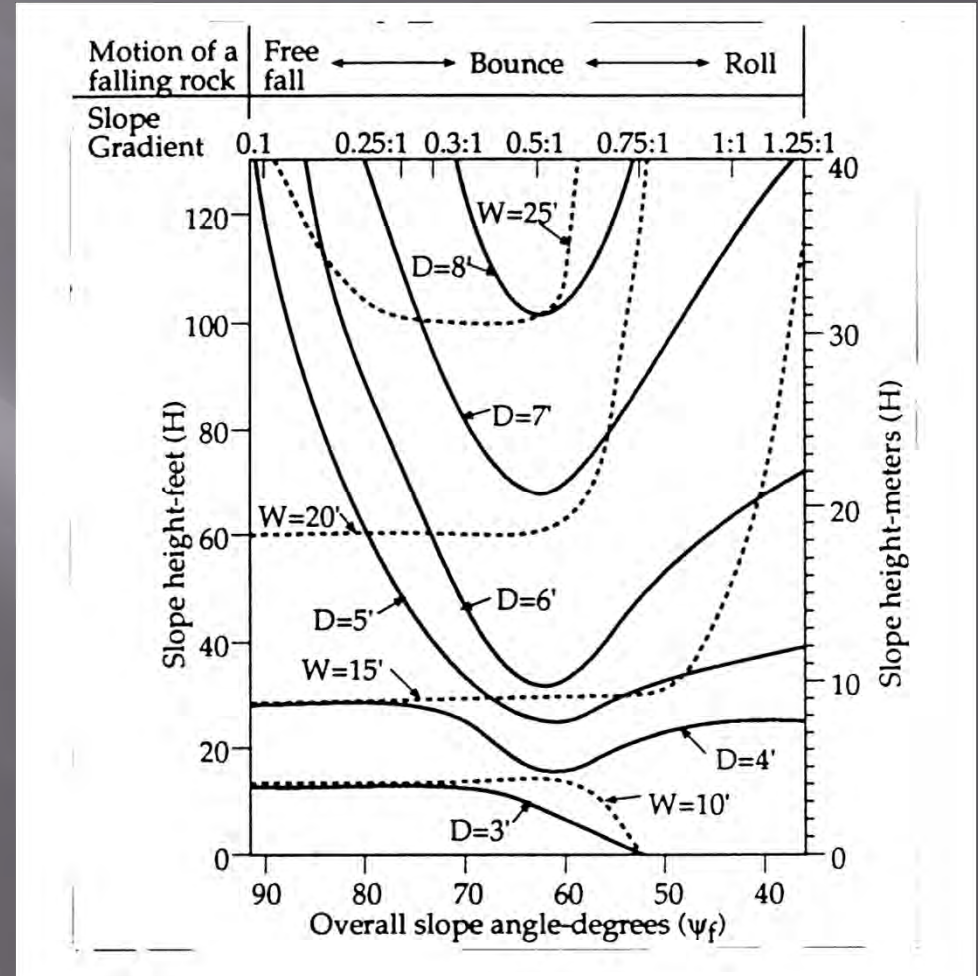
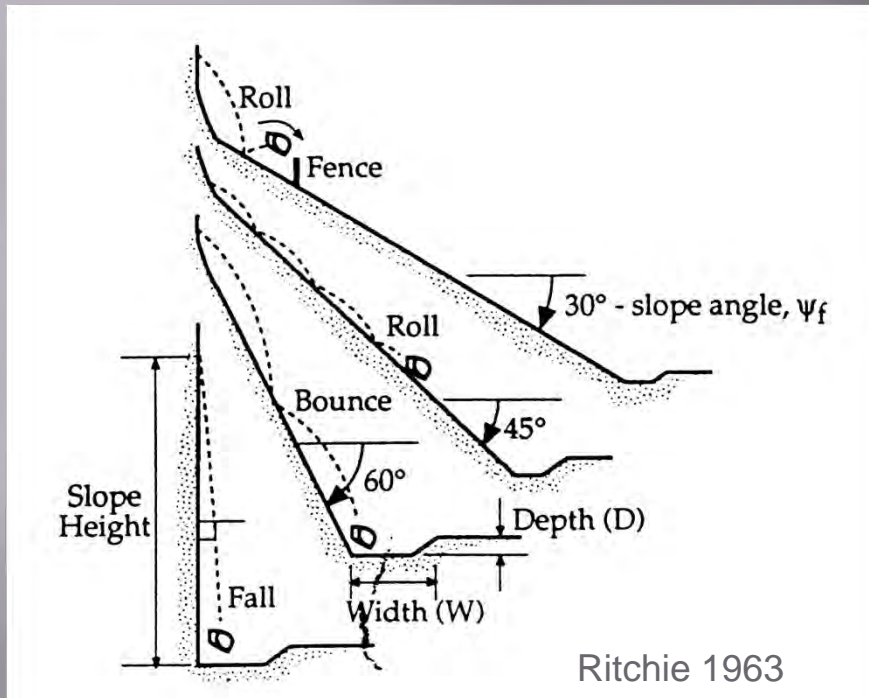


Protection Measures More Commonly Used in Mining

- ▣ Examination
- ▣ Restrict Access
- ▣ Equipment Position
- ▣ Benches
- ▣ Berms
- ▣ Computer Modeling
- ▣ Monitoring

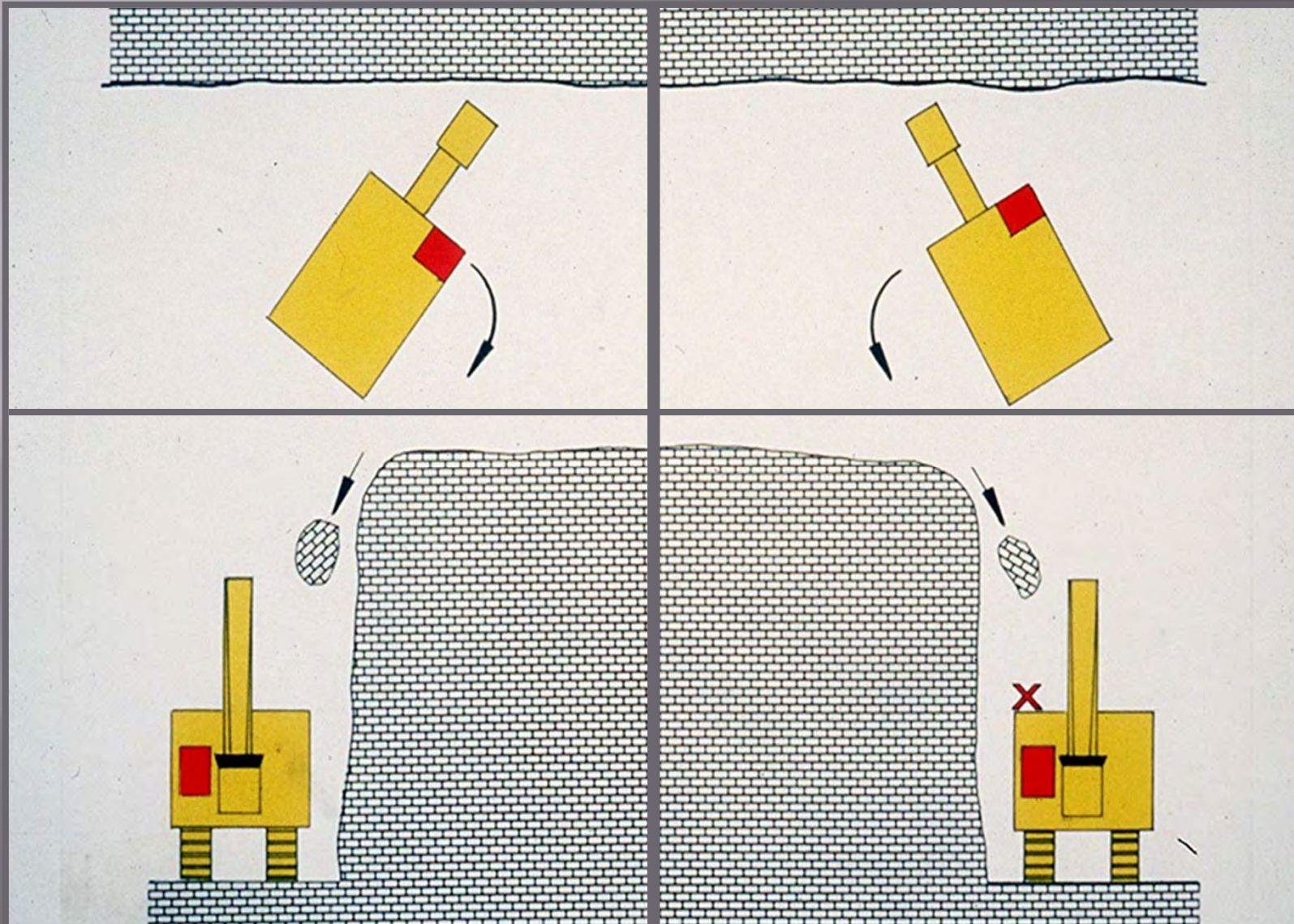


Rock Catch Ditches



Methodology can also be used to design berms.

Equipment Position Relative to the Highwall Face



Benches reduce the distance a rock can fall



Full Benches



Berm Containing Material



Berm Not Containing Material



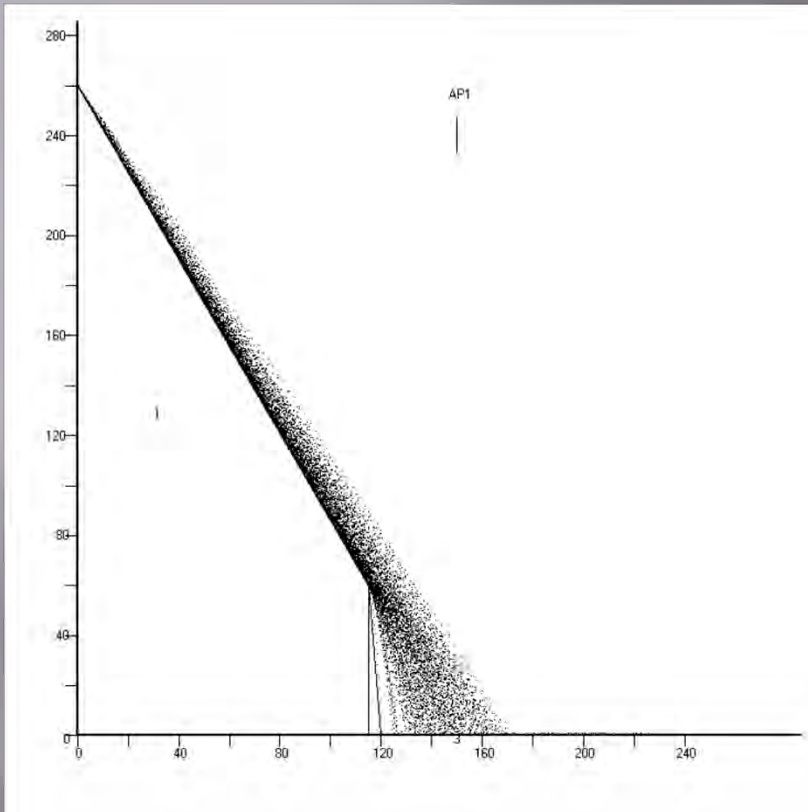
Is Berm Properly Sized and Located?



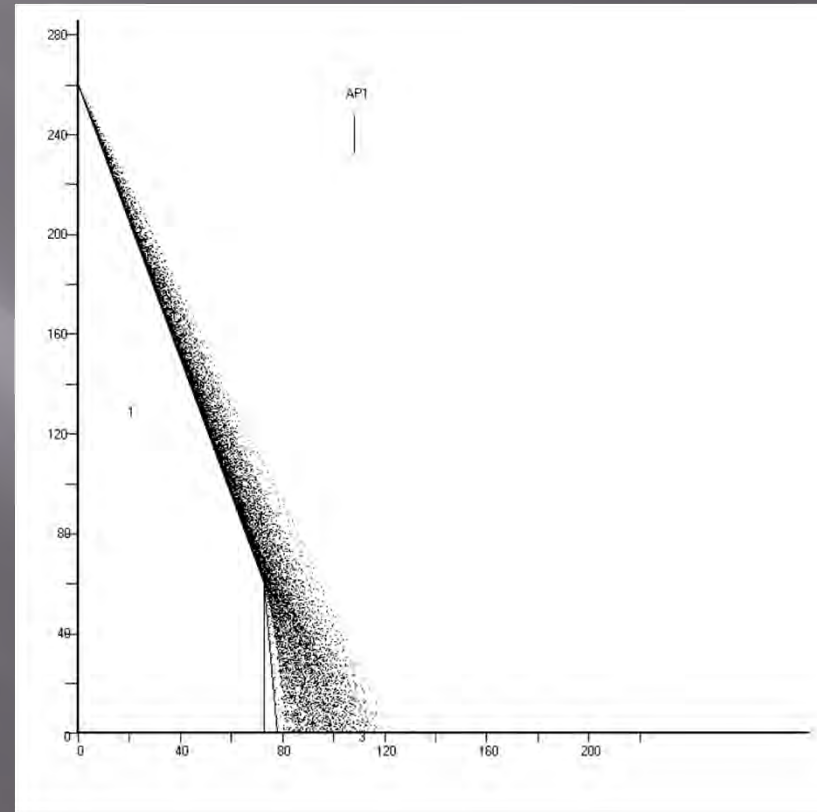
Computer Modeling

- ▣ Computer models such as the Colorado Rockfall Simulation Program (CRSP) can be used to design rockfall protection measures.
- ▣ Computer programs:
 - model field conditions,
 - apply random affects,
 - run many simulations, and
 - analyze patterns.

70-degree vs. 80-degree slope angles

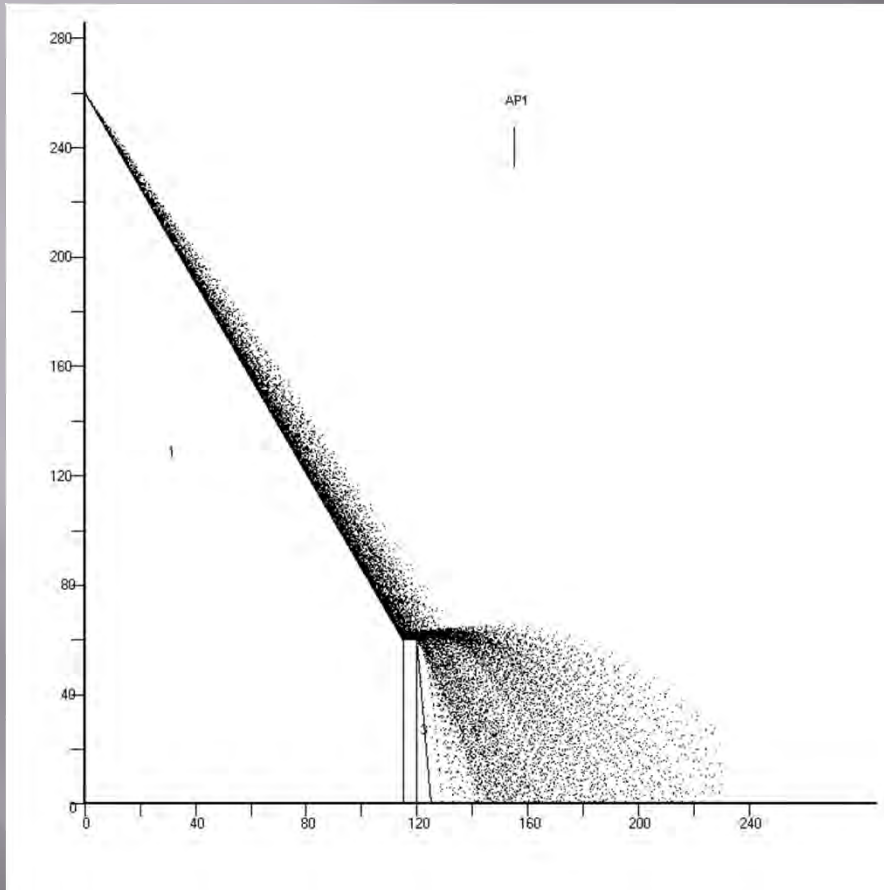


60 feet

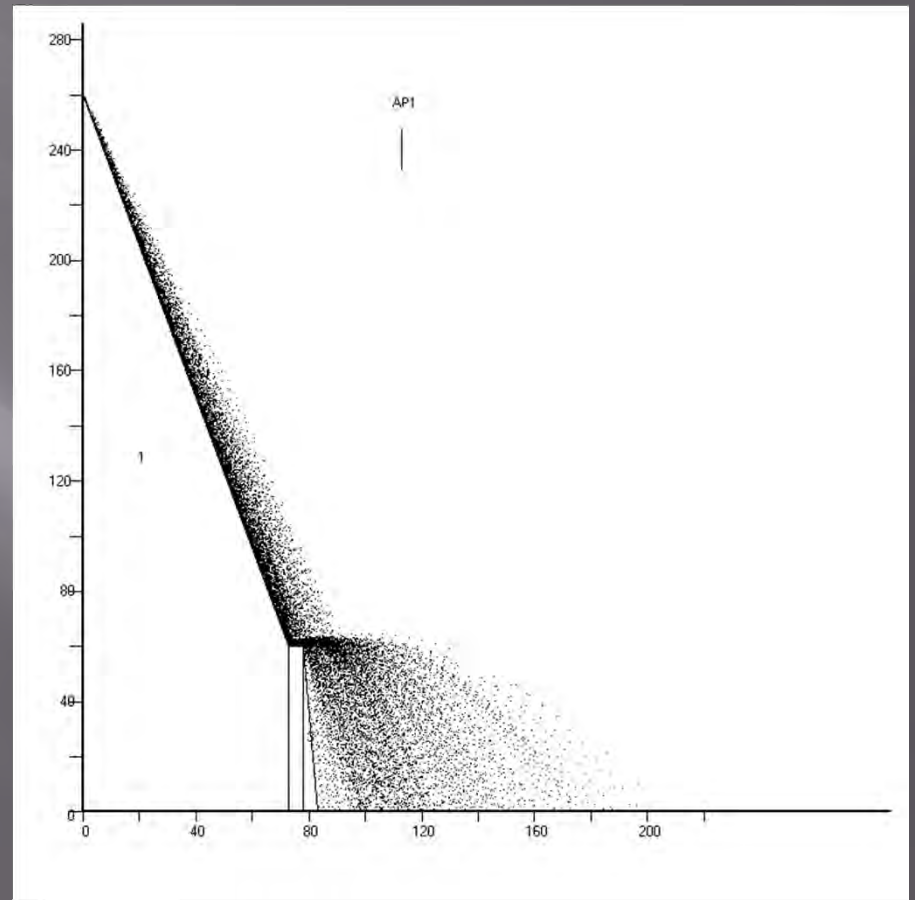


25 feet

Highwalls with a Ledge



120+ feet



120 feet

MSHA IS NOW REQUIRING THAT ALL SURFACE MINES SUBMIT A GROUND CONTROL PLAN TO ENSURE HIGHWALL STABILITY EXCEEDS A STATIC FACTOR OF SAFETY OF 1.3.

AFTER MUCH RESEARCH AND ANALYSIS, WE HAVE DEVELOPED A STABILITY MODEL WHEREBY WE CAN ANALYZE THE OVERALL FACTOR OF SAFETY FOR ALL HIGHWALLS.

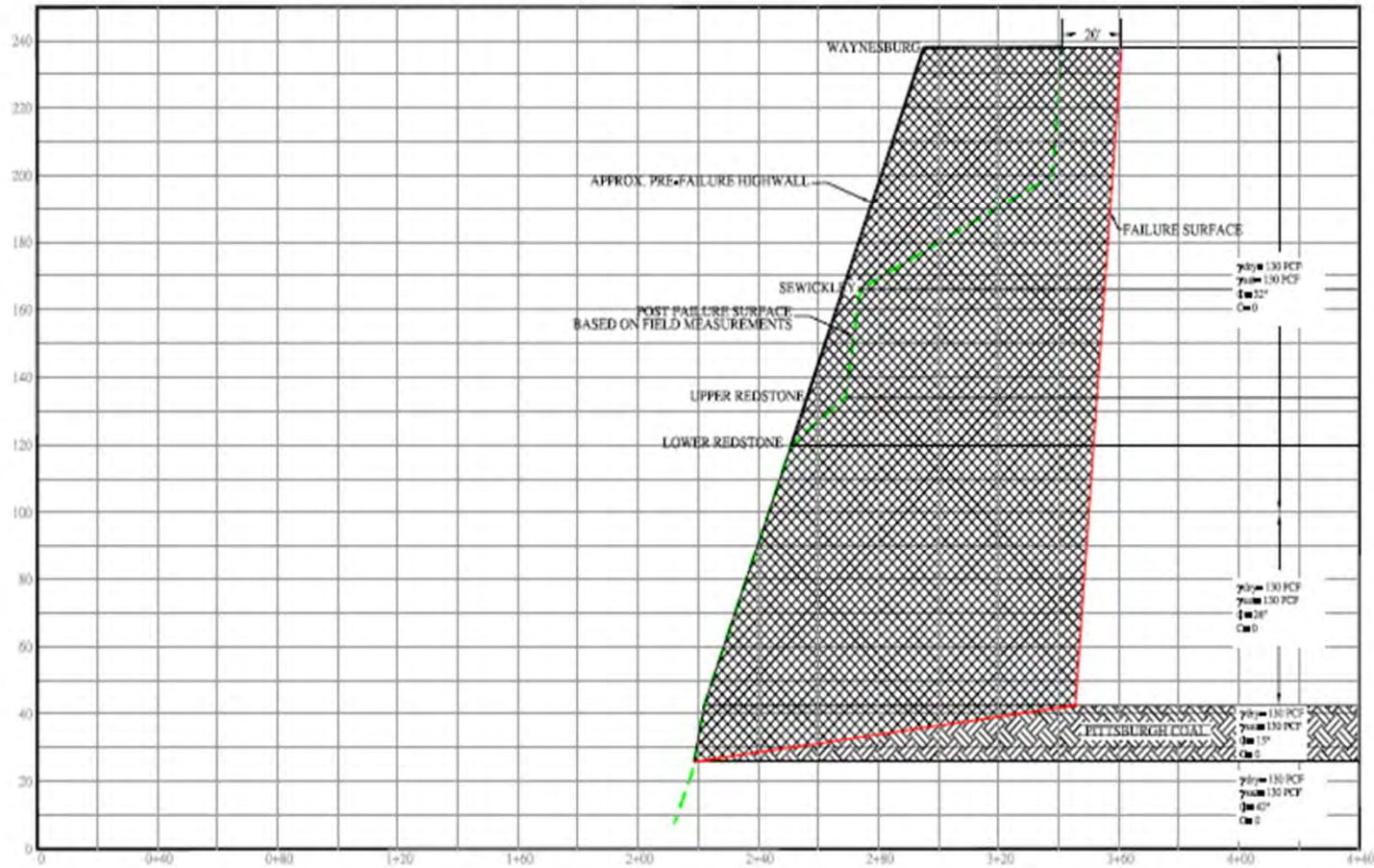
GENERAL INFORMATION



| | |
|-----------------|--------|
| Operator: | Tri-St |
| Mine: | Job # |
| Accident Date: | April |
| Classification: | Fall o |
| Location: | Dist. |
| | Coun |
| Mine Type: | Surfa |
| Employment: | 71 |
| Production: | 2,10 |

EXISTING MASS FAILURE

FACTOR OF SAFETY = 1.040



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Engineering Geology Design Challenges at the Soo Lock Replacement Project

**Infrastructure Systems Conference
25-29 July, 2007**



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Geologic Site Characterization – Bedrock Parameters

- **Bedrock strength parameters were established in accordance with EM 1110-1-2908 “Rock Foundations,” dated 30 Nov 1997 while utilizing:**
 - **Rock mechanics testing data**
 - Unconfined Compressive (elastic modulus & Poisson’s Ratio)
 - Anchor Bond Pull-out
 - Direct Shear Tests (intact, natural fracture, grout-on-rock)
 - Direct Tensile
 - Unit Weight
 - **Rock mass characteristics**
 - **Data from current and past exploration**
 - **Foundation reports of the construction of the Poe Lock**



Geologic Site Characterization – Bedrock Parameters

**US Army Corps
of Engineers**
Huntington & Detroit Districts

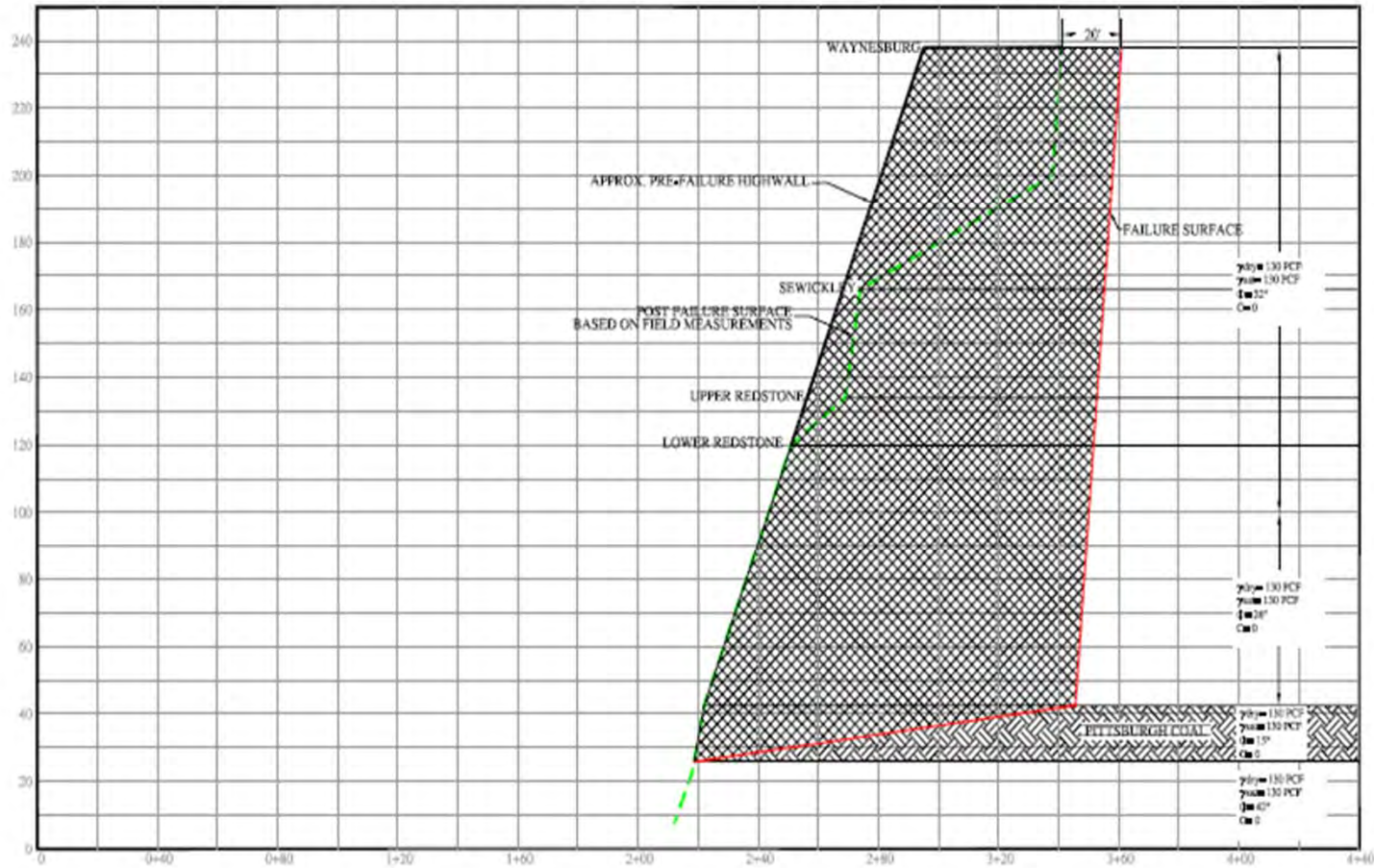
| Rock Unit | Sliding Friction | | Cross Bed Shear | | Allowable Bearing Capacity | Working Bond Strength | Modulus of Deformation |
|---------------------------------------|------------------|------|-----------------|------|----------------------------|-----------------------|------------------------|
| | ϕ | c | ϕ | c | | | |
| | deg. | psi. | deg. | psi. | | | |
| Hard Sandstone Members | 33 | 2 | 58 | 137 | 288 | 240 | 2.70 |
| Moderately Hard Sandstone Members | 23 | 2 | 47 | 68 | 230 | 168 | 2.26 |
| Shaly and Weathered Sandstone Members | 22 | 0 | 32 | 25 | 62 ¹ | 158 | 0.89 |
| Weak/Clay Seams | 21 | 0 | -- | -- | -- | -- | -- |

Note 1: 187 psi if Shaly and weathered Sandstone Members are confined and unexposed.

Bedrock Strength Parameter Values

EXISTING MASS FAILURE

FACTOR OF SAFETY = 1.040



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PITTSBURGH 50' BENCH ANALYSIS CASE 2

FACTOR OF SAFETY = 1.829



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References

- ▣ Broadbent and Zavodni (1982): Broadbent, C.D., and Zavodni, Z.M., "Influence of Rock Strength on Stability," Slope Stability in Surface Mining, Vol. 3, C.O. Brawner, ed., SME Littleton, CO, Chap. 2.
- ▣ Ritchie (1963): Ritchie, A.M., "Evaluation of Rockfall and its Control," Highway Research Record 17, Highway Research Board, NRC, Washington, D.C., pp13-28.
- ▣ TRB (1996): "Landslides Investigation and Mitigation," Special Report 247, Transportation Research Board, Washington, D.C.
- ▣ USDOT (1998): "Rock Slopes," FHWA HI-99-007, National Highway Institute, Federal Highway Administration, USDOT, Washington, DC
- ▣ **Miscellaneous POWERPOINT INFORMATION from Stan Michalek, P.E.**



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