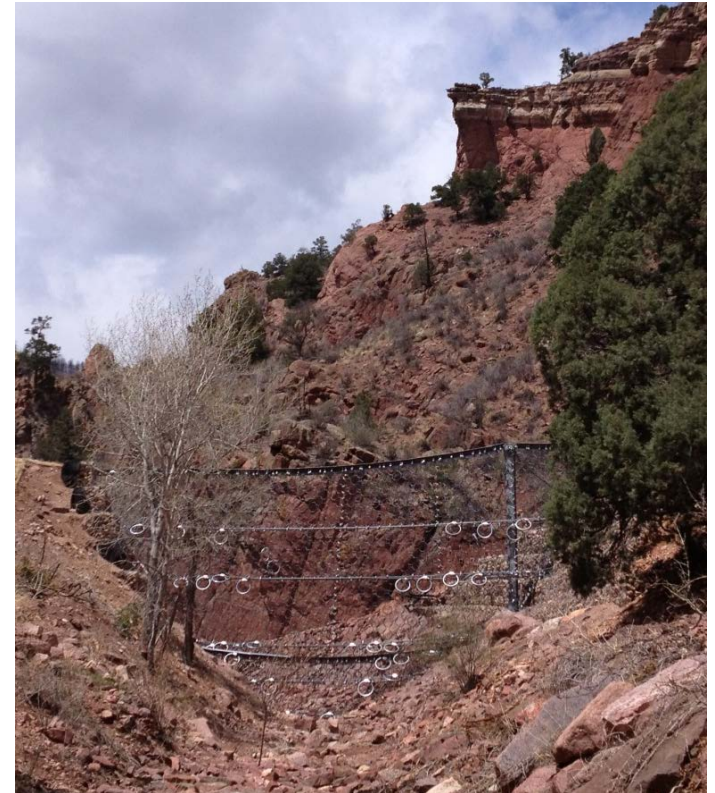


Analyses, Design, and Construction of Flexible Debris Flow Barriers in a Narrow Canyon



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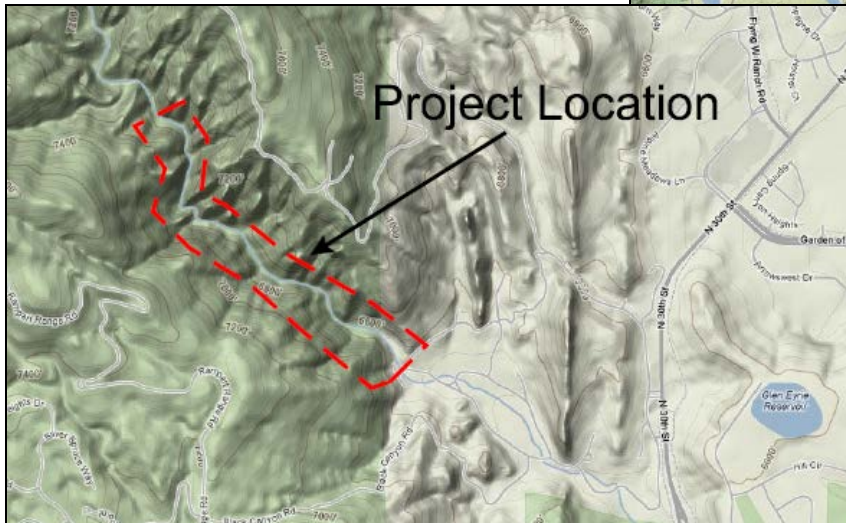
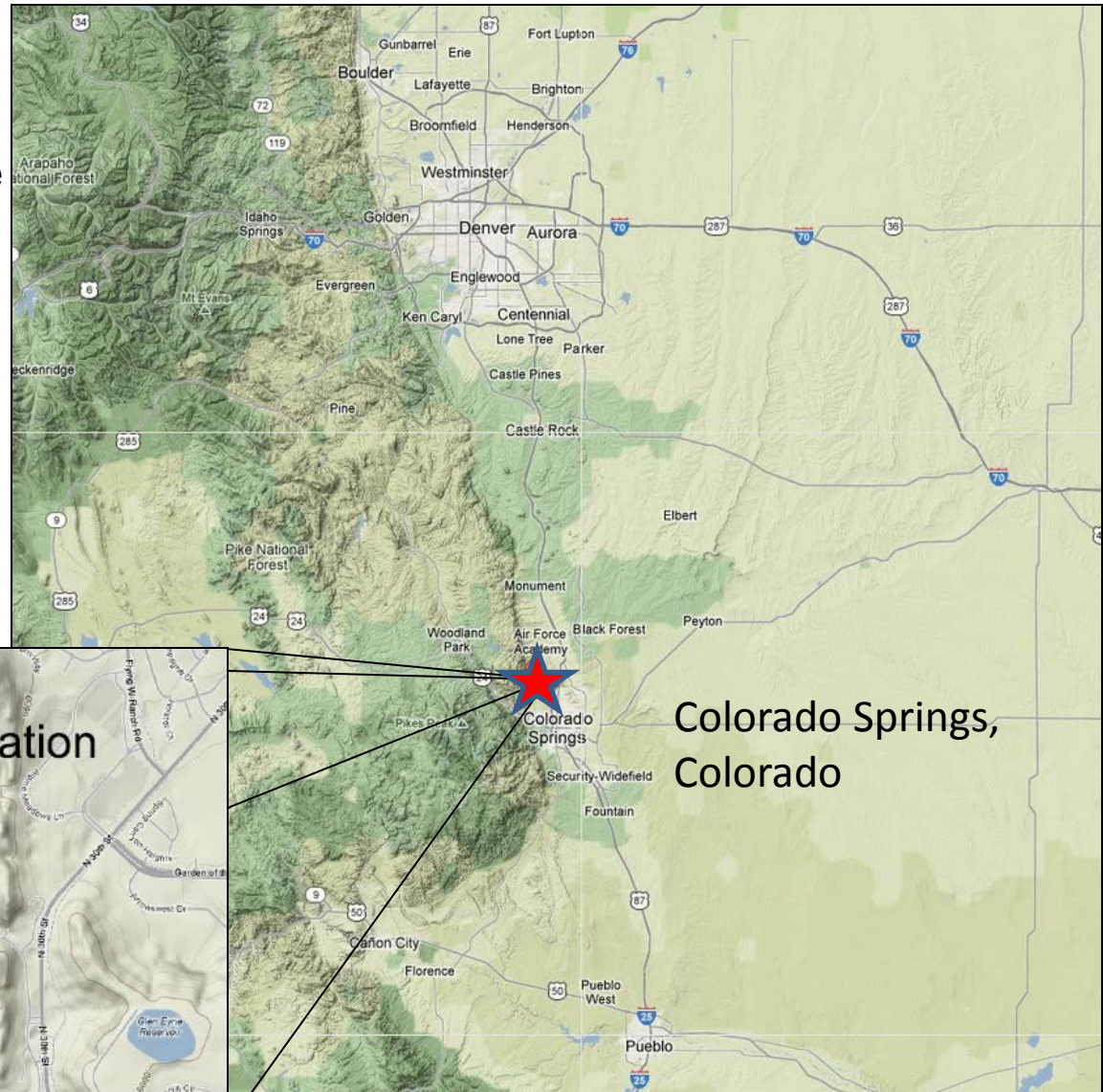
13th Annual Forum
Geohazards Impacting Transportation in
the Appalachian Region
Harrisonburg, Virginia
July 30-August 1, 2013

- **Derek Strickler, The Navigators**
Colorado Springs, Colorado
- **Midwest Rockfall, Inc.**
Henderson, Colorado
- **John Kalejta, Geobrugg Geohazards Solutions**
Rocky Mountains Region



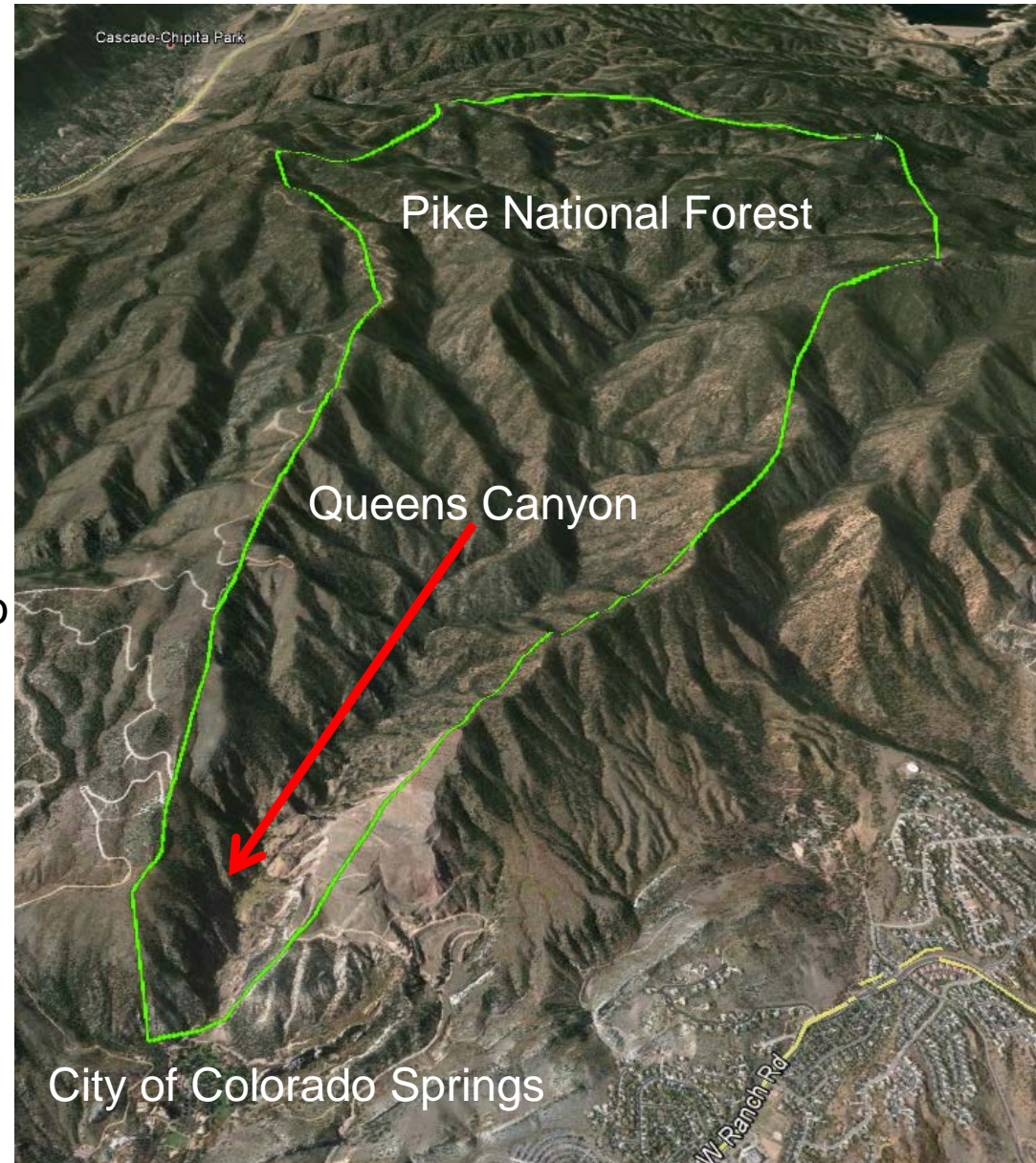
Introduction

- Colorado Springs, Colorado
- Rocky Mountains Front Range
- Camp Creek Watershed
 - (11.2 square miles)
- Private Property
- Between USFS and City land



Site Description

- Camp Creek Watershed
 - 11.2 square miles
- Severely burned by the Waldo Canyon Fire Summer 2012
- Upper Watershed- USFS Property
- Queens Canyon- Private Property
- Lower Watershed- City of Colorado Springs

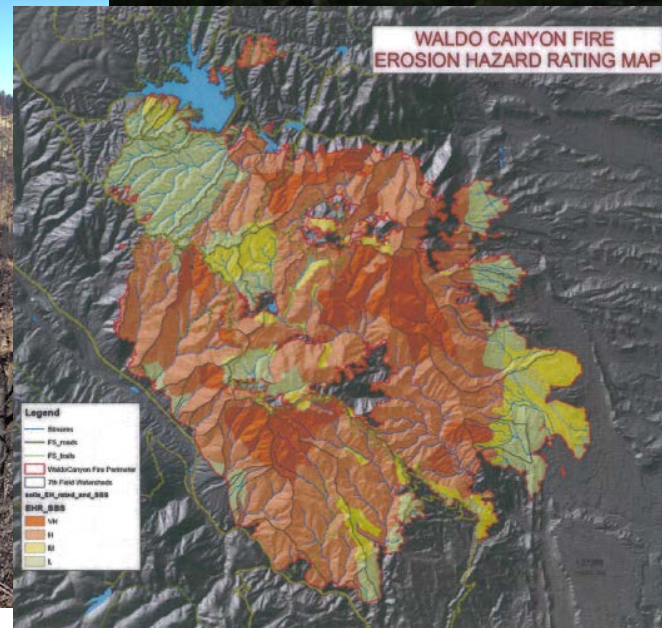


Waldo Canyon Fire

- Fire Started: Saturday, June 23, 2012
- Fire Contained: Tuesday, July 10, 2012
- Total Acres: 18,247

Ownership

National Forest – 14,422 acres
Department of Defense – 147 acres
Private – 3,678 acres



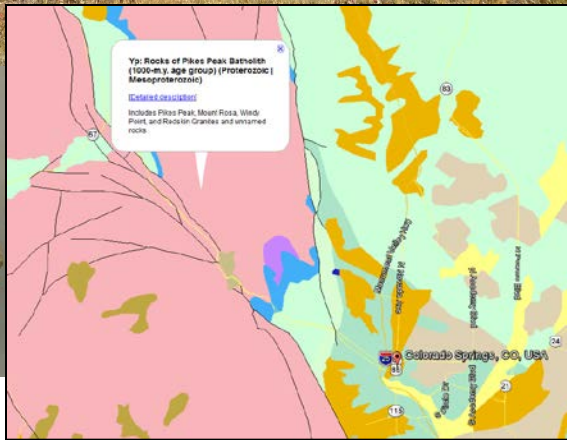
Post-Fire GeoHazards

Manitou Springs Mudflow Event

Post Waldo Canyon Fire



Pikes Peak Granite



Channel morphology and gradient dictates available volume of storage!



Potential Debris Flow Barrier sites are identified in the project area.

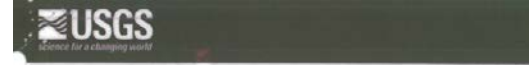
Sites are chosen based upon:

- storage potential for debris
- protection of critical infrastructure
- ability to clean-out



Using the results from the field investigation and USGS report on Waldo Canyon Fire:

- Volume of expected debris are determined
- Geological characteristics of debris flows are determined
- Geobruigg DEBFLOW software is utilized to analyze loading of debris flow barriers



Prepared in cooperation with Colorado Department of Transportation

Probability and Volume of Potential Postwildfire
Debris Flows in the 2012 Waldo Canyon Burn Area
near Colorado Springs, Colorado



Table 2: Probability of a debris flow initiating during a 10 year storm (a 10% chance of occurrence in a given year) (Design Storm)

Drainage or Subwatershed with High Probabilities	Probability *based on Initial BS	Volume (m3)
10 (N-Douglas)	41	57,000
12 (L -Queens Canyon)	45	>100,000
13 (K - Williams)	54	77,000
14 (H - Waldo)	53	48,000
15 (G - unnamed)	74	14,000

The USGS estimated a total debris flow volume of >100,000 m³ for a 10 year storm event!

Using field data and literature references:

- Input parameters are chosen for debris flow analyses
- DEBFLOW software models static and dynamic characteristics of debris flows and outputs a design barrier size

GT12-26 Glen Eyrle Debris Flow Barriers Site S-2 Channel

Dimensioning of the flexible Debris Flow Protection System GEOBRUGG VX/UX - DEBFLOW

Input Parameters

Type and density of the debris flow

	Type	Load case 1	Load case 2	Load case 3
Type of debris flow (granular or mud flow)		granular	no load case	no load case
Density of the debris flow material	$\rho =$	2000		[kg/m ³]
Specific weight of the debris flow material	$\gamma =$	19.6		[kN/m ³]
Water content	$\omega =$	0.39		-

Debris flow volume and number of surges

		Load case 1	Load case 2	Load case 3
Total debris flow volume (incl. water)	$V_{tot} =$	1000		[m ³]
Number of surges	$N =$	5		-
Volume per surge (average)	$V_{av} =$	111		[m ³]
Volume of first surge (recommended)	$V_{v1,rec} =$	167		[m ³]
Volume of first surge (chosen)	$V_{v1} =$	170		[m ³]

Peak discharge

		Load case 1	Load case 2	Load case 3
Peak discharge (acc. to Rickenmann)	$Q_{p,rec} =$	7.4		[m ³ /s]
Peak discharge (chosen)	$Q_p =$	7		[m ³ /s]

Safety factor

Global safety factor	$SF =$	1.4		
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GT12-26 Glen Eyrle Debris Flow Barriers Site S-2 Channel

Barrier Location No. 1

Geometry of barrier location

System height	$H_{b,1} =$	2.4	[m]
Width of torrent on the level of the bottom support ropes	$b_{b,1} =$	4	[m]
Width of torrent on the level of the top support ropes	$b_{t,1} =$	12	[m]
Distance to the next barrier upstream	$L_{b,1} =$	500	[m]

Torrent inclination and retention volume

System height of the filled barrier	$H_{f,1} =$	1.8	[m]
Average torrent inclination upstream of the barrier	$i_{t,1} =$	14	[%] 8°
Deposition inclination of filled barrier (acc. to Rickenmann)	$i'_{t,1,rec} =$	9.3	[%] 5°
Deposition inclination of filled barrier (chosen)	$i'_{t,1} =$	9	[%]
Angle between ring net and river bed	$\xi =$	87.0	[°]
Length of deposited material behind barrier	$L_1 =$	36.5	[m]
Retention volume	$V_{r,1} =$	262	[m ³]

Front velocity and flow height

		Load case 1	Load case 2	Load case 3
Front velocity (acc. to Rickenmann)	$V_{1,base} =$	2.7		[m/s]
Front velocity according to Strickler ($v_{1>vstr}$)	$vstr =$	2.9		[m/s]
Impact velocity at barrier location (chosen,max. v-value)	$V_1 =$	2.9		[m/s]
Flow height	$h_{f,1} =$	0.6		[m]
Recommended max. basal opening height (acc. to Wendeler)	$h_{b,1} <=$	0.4		[m]

Flexible, permeable debris flow protection system

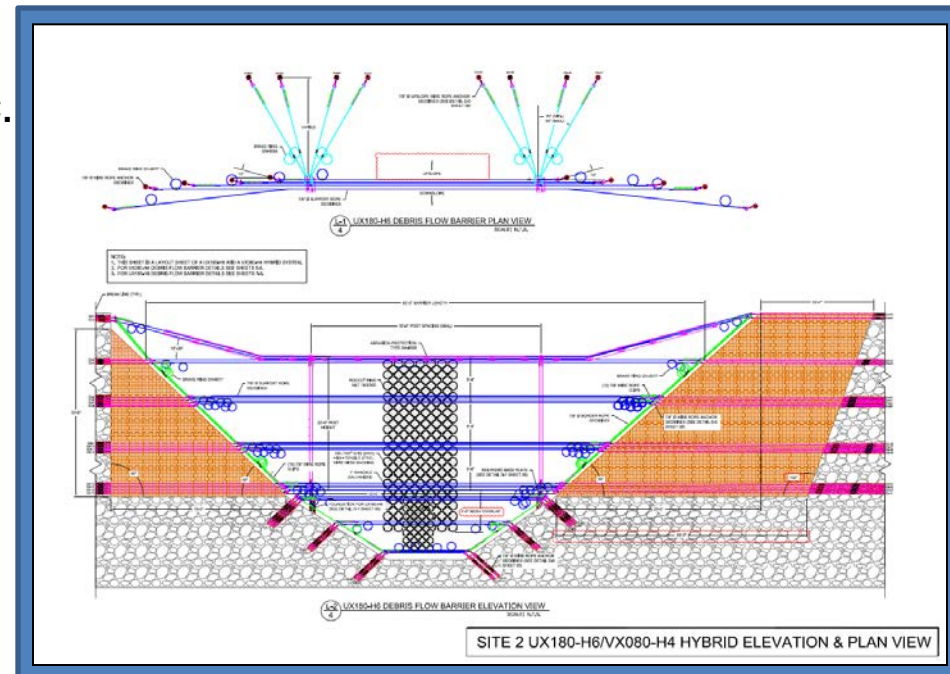
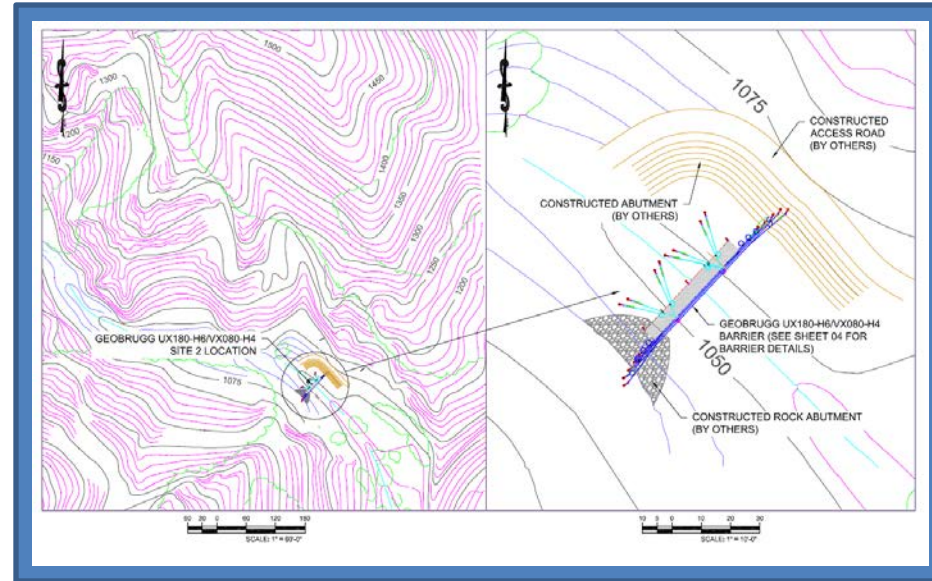
System type	Type	GEOBRUGG VX080-H4
Max. system height	$H_{b,max} =$	4.4 [m]
Max. system width above	$b_{a,max} =$	15 [m]
Max. system width below	$b_{u,max} =$	8 [m]
Proof of system height and system width		fulfilled!

Proof of max. dynamic loading (stopping)

		Load case 1	Load case 2	Load case 3
Width factor (width at barrier location to standard width)	$BF_1 =$	0.80		
Dynamic loading (Pressure and impulse acc. to Wendeler)	$MD_{dyn,1} =$	24		[kN/(m ² ·s ²)]
Resistance against dynamic loading	$RD_{dyn,1} =$	60		[kN/(m ² ·s ²)]

Phase 2 Results

- 2 Barrier Locations were chosen for construction
- **KANE** GeoTech produced engineered drawings for Geobrugg UX and VX debris flow barriers
- Client put the project out to bid
- Pre Bid meeting held to familiarize contractors with project, stress tight completion timeframe
- Project awarded to Midwest Rockfall, Inc. on January 30
- Final Completion Deadline: March 30



Construction Begins



Helicopter Transport of Materials and Equipment



Helicopter Transport of Materials and Equipment



Anchor Drilling



Grouting Anchors



Anchor Pull Testing



Anchor Pull Testing



Assembly of Barriers



Assembly of Barriers



Completion – Site 2 UX120-H6 Debris Flow Barrier



Completion - Site 2 UX180-H6 & VX080-H4 Debris Flow Barriers



Successful Retention of Debris Flow



July 1, 2013



Successful Retention of Debris Flow



July 1, 2013



A planned, phased approach enabled timely, effective completion:

- A thorough initial investigation produced engineered drawings and bid documents
- Rapid selection of a qualified contractor and daily oversight
 - Debris flow mitigation systems installed on time and before spring rains
- On-site engineer's representative
 - Allowed effective testing of anchors
 - Kept costs low for the contractor and client



Thanks for your attention!